





BCR TEAM INTRODUCTION

Community Partners

Journey Women's Center - Amy Voth

Industry Partners

Guaranteed Watt Saver – Kelly Parker 820 Solar – Cory Baitz **Standard Panel – John Pardue AWAD Construction** Dolese Lee Glass and Window

Special Thanks

Homestead School - Bruce & Barbra Johnson

Instructors

Khaled Mansy, Ph.D. – Architecture Jay Yowell, AIA – Architecture **Christian Bach, Ph.D. – M. Engineering** Hebatalla Nazmy, Ph.D. – Interior Design



Christian Brack Architecture



Maggie Carathers Architecture



Whitney Waitsman Architecture



Abigail Richardson Architecture



Jahnia Wright Interior Design



Amr Abdelmoneim Mechanical Engineering





Emily Smith Architecture



Ian Strickland Architecture



Lia Jenson Interior Design



Pouria MoghimiGhadikolaei Mechanical Engineering

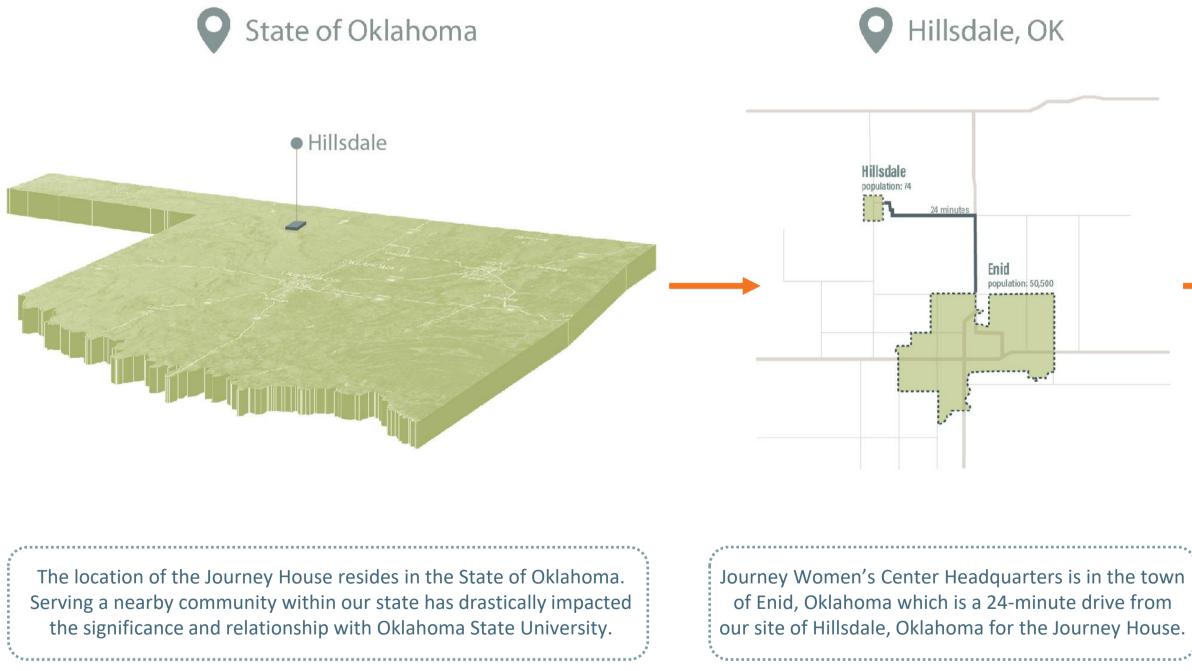


Jacob Gore Architecture



Molly Hoback Team Lead, Architecture

H C R SITE CONTEXT









The illustrated site focuses in on the intersection of streets in Hillsdale. Unit A and B of the Attached Housing project are displayed as well as the additional transitional Units C & D.

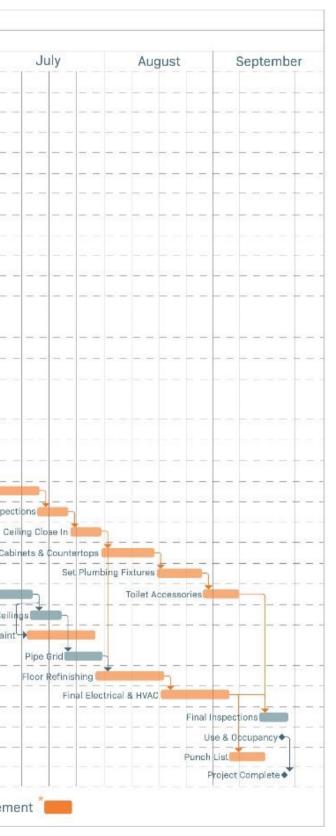
BUDGET & TIMELINE

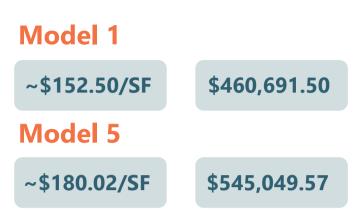
		Solar Decathlon Journey Women's Center Construction Timeline						
2 Construction Phase							125 100 400	1
1.222.54	I the second I	January	February	March	April	May	June	
Task	Days							_
1 Document Review & Revision		ent Review & Revision						_
2 Mobilization & Layout	3 days	Mobilization & Layout						_
3 Bid & Contracts	10 days	Bids & Contracts	h					_
4 Foundation Design	10 days	Foundation Desig						_
5 Reinforce Foundation	20 days	Reinfo	nce Foundation					
6 Concrete Slab	28 days			Concrete Slab				
7 Plumbing & Electrical Underground	15 days	Plumbing & Electric	al Underground					
8 Wood Framing	48 days							
9 Shop Drawings	33 days	Shop Drawings*		1				
10 Installation of Wood Framing	15 days			Installation of Woo	d Framing			
11 Roofing	27 days							
12 Design Roof Framing	30 days		Design of Roof Fram	ning *				
13 Install Roofing	15 days			Instal	Roofing			
14 Set up Roof Equipment	2 days			Set	Up Roof Equipment			-
15 HVAC Rough In	20 days		HVAC	Rough In				
16 In-Wall and Underfloor Rough-Ins	10 days				n Wall and Underfloor Ro	ugh-Ins		
17 Wall Close In Inspection	1 day				Wall	Close in Inspection		
18 Insulate, Drywall & Finish	20 days				Sins	sulate, Drywall, & Finish	*	
19 Frame Ceilings	5 days					Frame	e Ceilings	
20 HVAC & Electrical work to Grid	12 days						Electrical work to Grid	-
21 Ceiling Close In Inspection	1 day						Ceiling Close In In	nspe
22 Ceiling Close In	4 days							C
23 Cabinets & Countertops	3 days							Ca
24 Set Plumbing Fixtures	5 days							-
25 Toilet Accessories	5 days					Door	s, Frames, & Hardware	
26 Doors, Frames, & Hardware	7 days						Paint Exposed	d Ceil
27 Paint Exposed Ceilings	4 days							
28 Wall Paint	12 days							
29 Pipe Grid	3 days		+ - + - +					
30 Final Electrical & HVAC	8 days				명이지 모이지 고려가 같아?			1
31 Final Inspections	3 days							
32 Use & Occupancy	3 days							-
33 Punch List	7 days							-
34 FINISH PROJECT	0 day							-

Solar Decathlon Journey Women's Center Construction Timeline

Figure 1.4: Gantt Chart Timeline for Construction Phase







A cost the client can afford. Land is donated. SIPs are donated. 30% rebate on PV.

Model 1

36 weeks

Model 5

30 weeks

A net saving of 6 weeks.

If we were to start construction in January of 2025, the estimated end date would land at the end of September totaling 36 weeks. However, with the integration of SIPs Panels, it would reduce the total construction time by 6 weeks.

H C R TARGET MARKET

295+

195+

ULTRASOUNDS GIVEN

225+

495+

"Journey Women's Center educates, supports, and empowers women facing unplanned pregnancies with compassionate, professional care."

Services

No-Cost Limited OB Ultrasounds

Purpose of Design

+ The maternity home will provide housing for 4 women and house parents in each unit

Options Counseling + The goal of the maternity home is to provide safe housing and an encouraging environment for women "Oklahoma has the second highest teen pregnancy rate in the nation."

(FocusForwardOK)

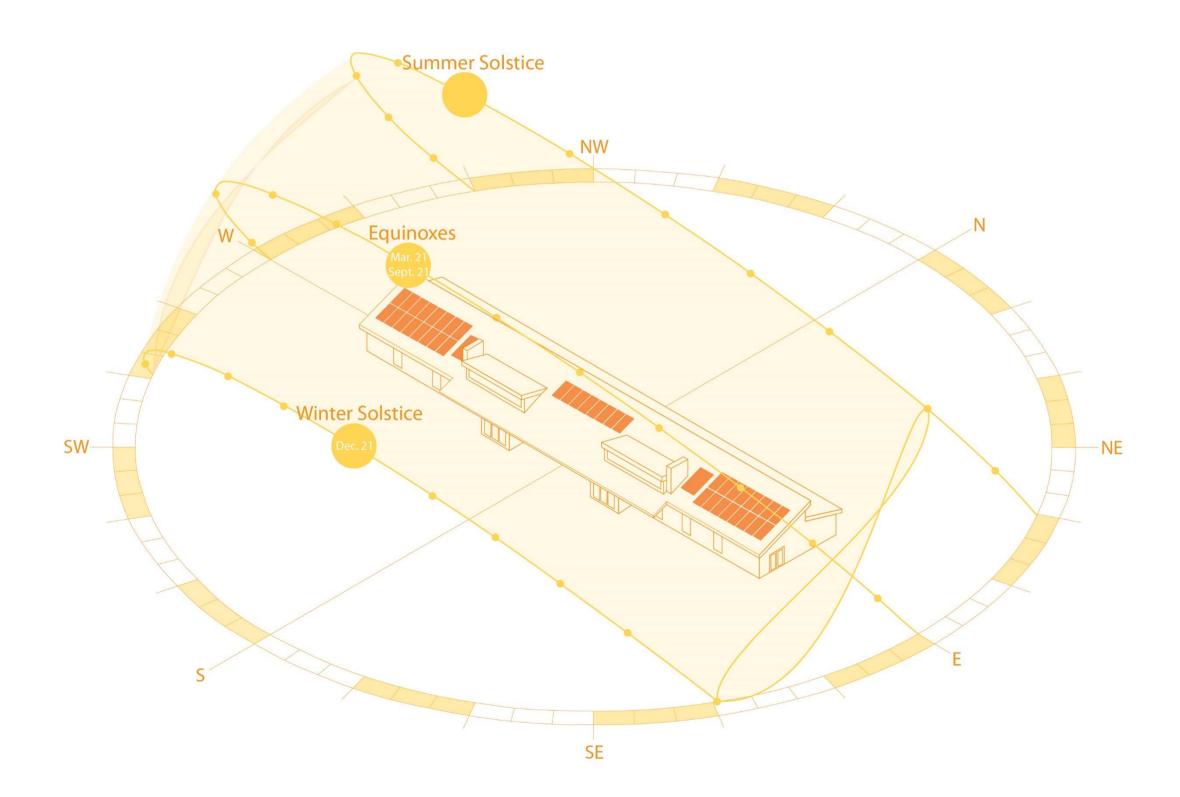
No Cost Pregnancy Tests

+ Women can live there during pregnancy all the way until the child is 1 year old

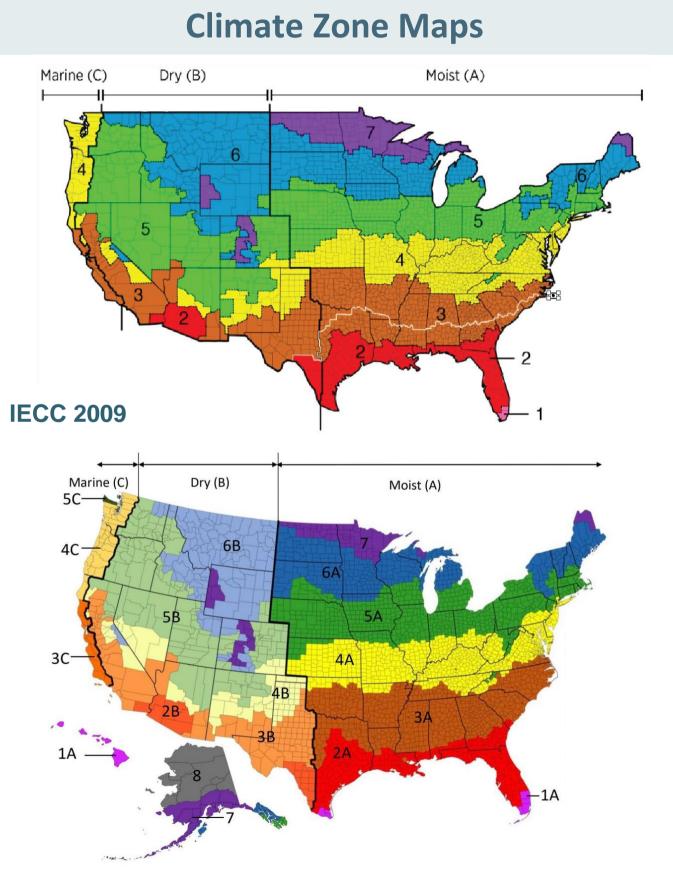




Sun Path Diagram

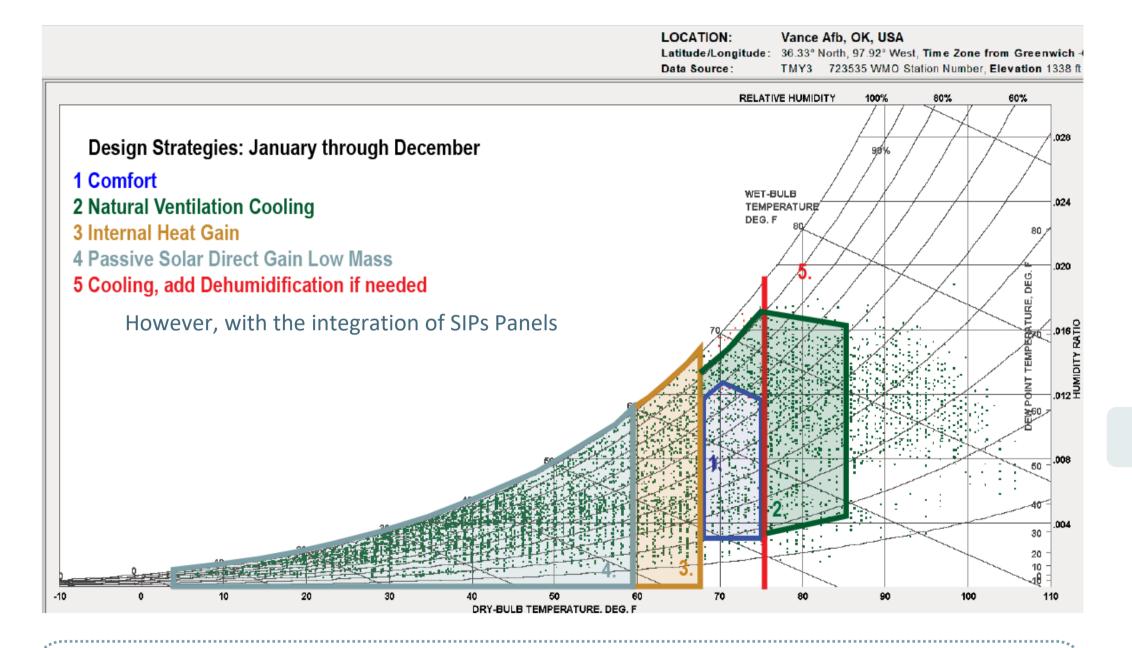






IECC 2021

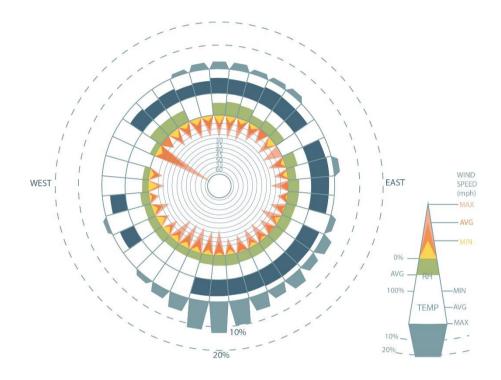
Psychrometric Chart - Hourly



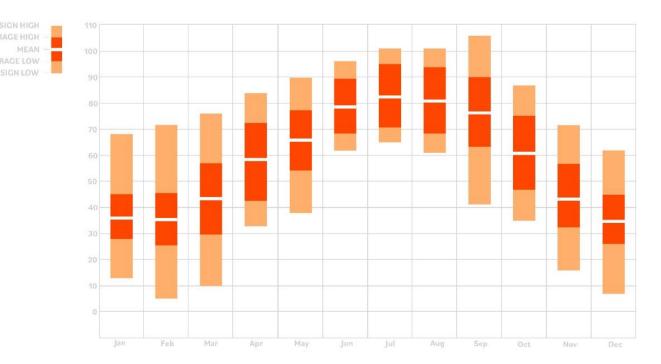
According to IECC 2021, Hillsdale, Oklahoma is located within Climate Zone 4A. Temperature range helped us in the design of passive solar heating, and the wind wheel helped us to design the natural ventilation and the fan-assisted ventilation. Our climate provides a **high potential** for passive heating and cooling. Additionally, resources such as the Psychrometric chart provided guidance in our desired condition of the air. The utilization of the Sun Path Solar Diagram allowed us to develop the necessary overhangs and window openings.



Psychrometric Chart - Hourly



Temperature Range



BUILDING CODES & STANDARDS

Building Codes

Energy Code IECC 2009, IECC 2021, RESNET 301 (2019)

Envelope Values

Building Code

IBC 2018 (R-2), IRC 2009, IRC 2021 Building Classification & Req's

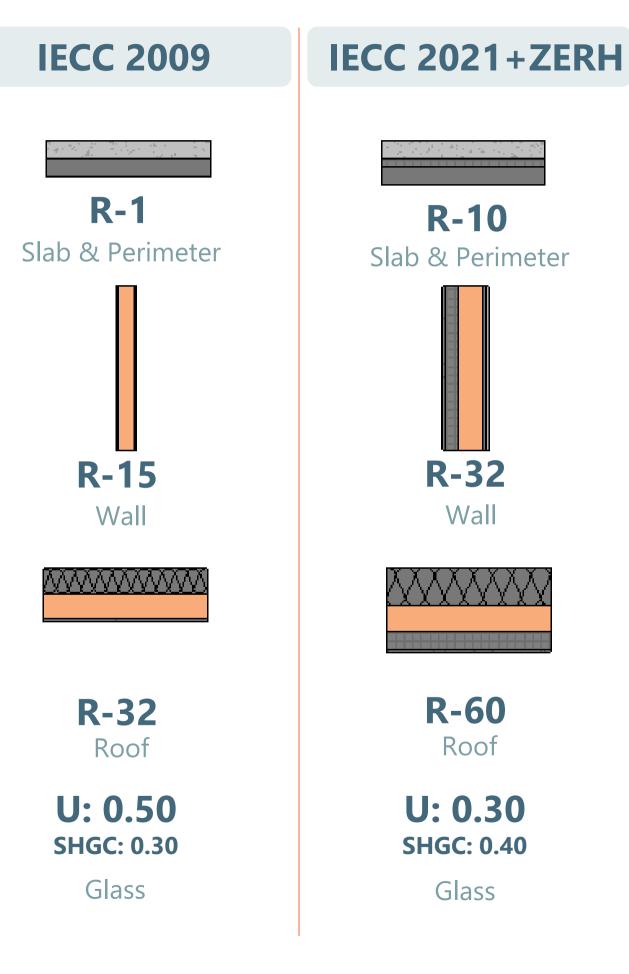
Mechanical Standard

ASHRAE 62.2 (2019), 90.2 (2018), 228 (2019), 55.2 (2017), 227P (2023), ACCA Manual S & J

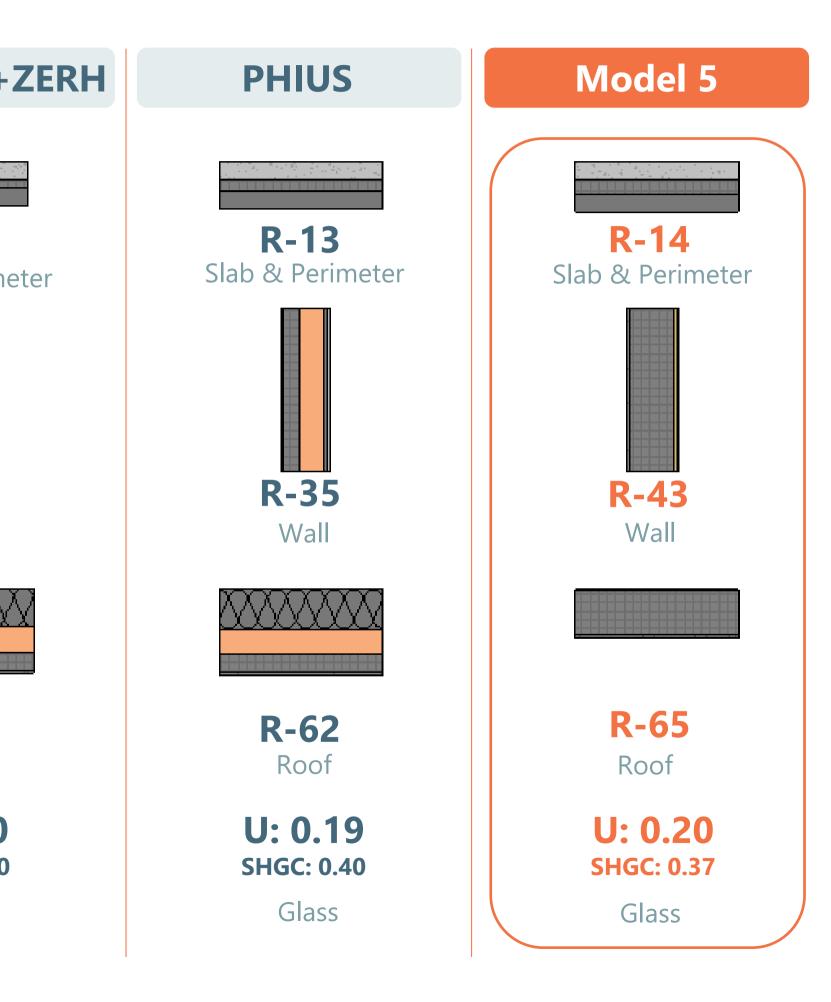
System Sizing & Ventilation

Standards & Programs

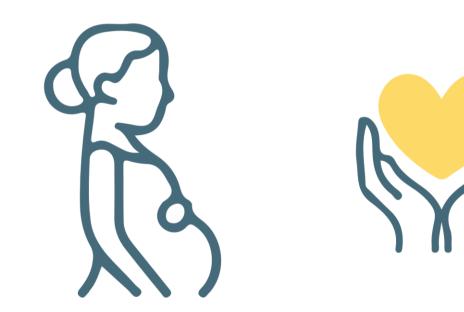
DOE ZERH, Phius, WELL Envelope Values & Best Practices







H C R DESIGN GOALS



Норе

Community



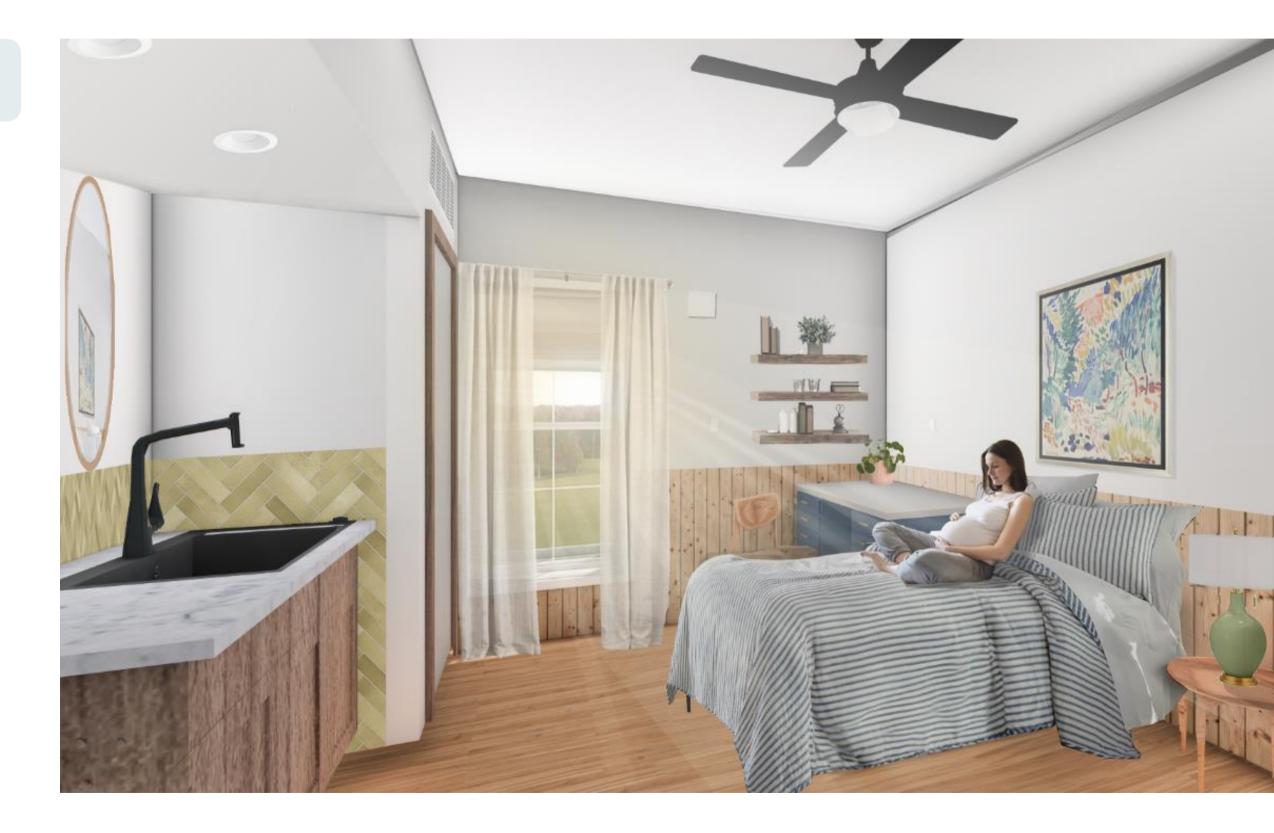


Resiliency

HCR DESIGN GOALS

Норе

- + 24/7 Care
- + Biophilic design
- + Natural light / shadow-free daylighting
- + Positive environment for healing & gaining life skills
- + Open views to outside
- + Rural living
- + Community greenhouse





B C R DESIGN GOALS

Community + Design Justice

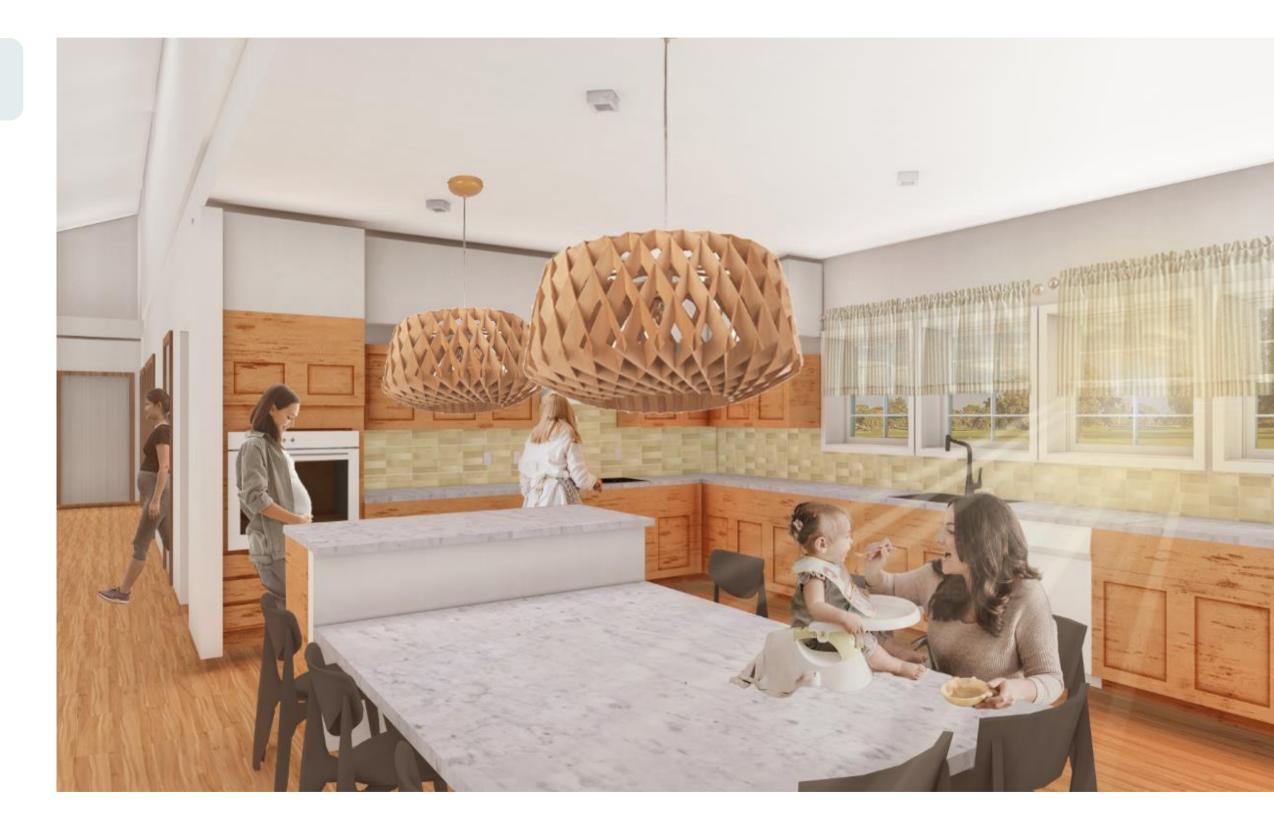
- + Local support
- + Cluster design
- + Funds from Enid/Hillsdale
- + Site donated by community member
- + Outdoor living
- + Open plan and shared bathrooms





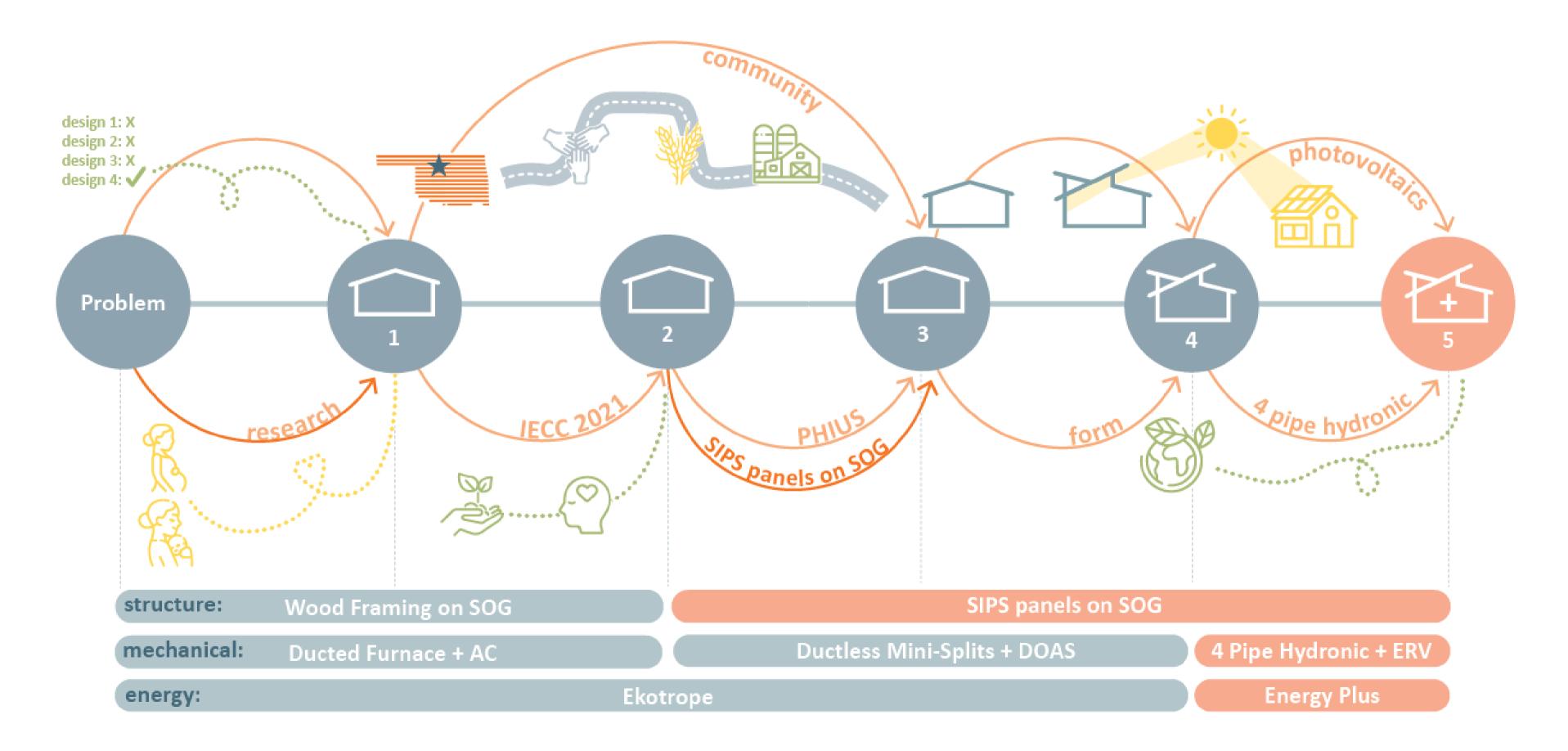
Resiliency + Sustainability + Climate Action

- + Sustainable materials
- + Passive systems
- + PV & Battery storage
- + Natural ventilation
- + Solar water heating with 80-gallon tank & backup electric coil/heating
- + FEMA-Approved above-ground storm shelter, easily accessible & close to exterior wall
- + Vegetable garden
- + Future community wind power





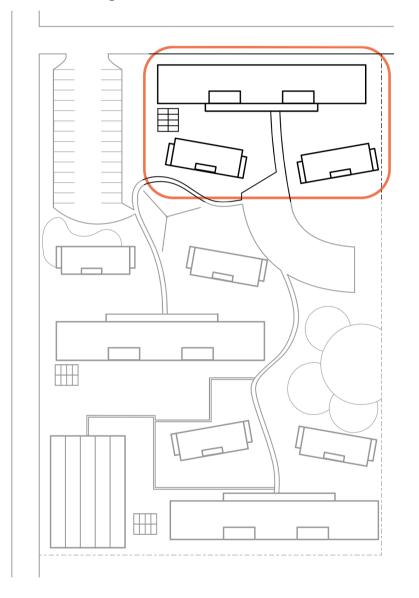
B C R DESIGN METHODOLOGY





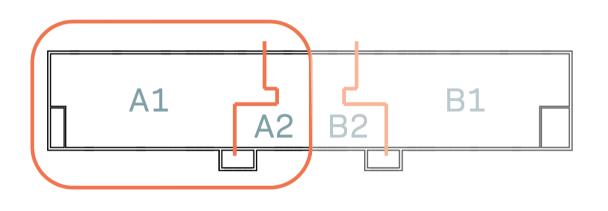
Phase 3

A Compound of 3 Clusters



Phase 2

The North Cluster: Units A + B = Maternity Homes Units C + D = Transitional Units





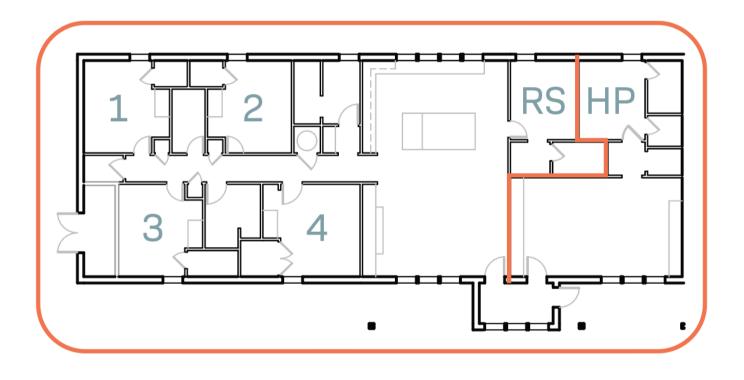


Site EUI Site EUI Climate **4 Units** 5,980 SF **After PV: Before PV:** Zone: -2.81 9.64 **4**A 2 Maternity Units **12 Bedrooms** kBtu/SF/yr kBtu/SF/yr **2 Support Units 8 Bathrooms**



Phase 1

4 Dwelling Units: A1 + A2 + B1 + B2



HERS **HERS** Annual **After PV: Before PV: Savings**: A1 = -1A1 = 26 \$1,248 A2 = -3A2 = 27

CONTESTS DISCUSSION

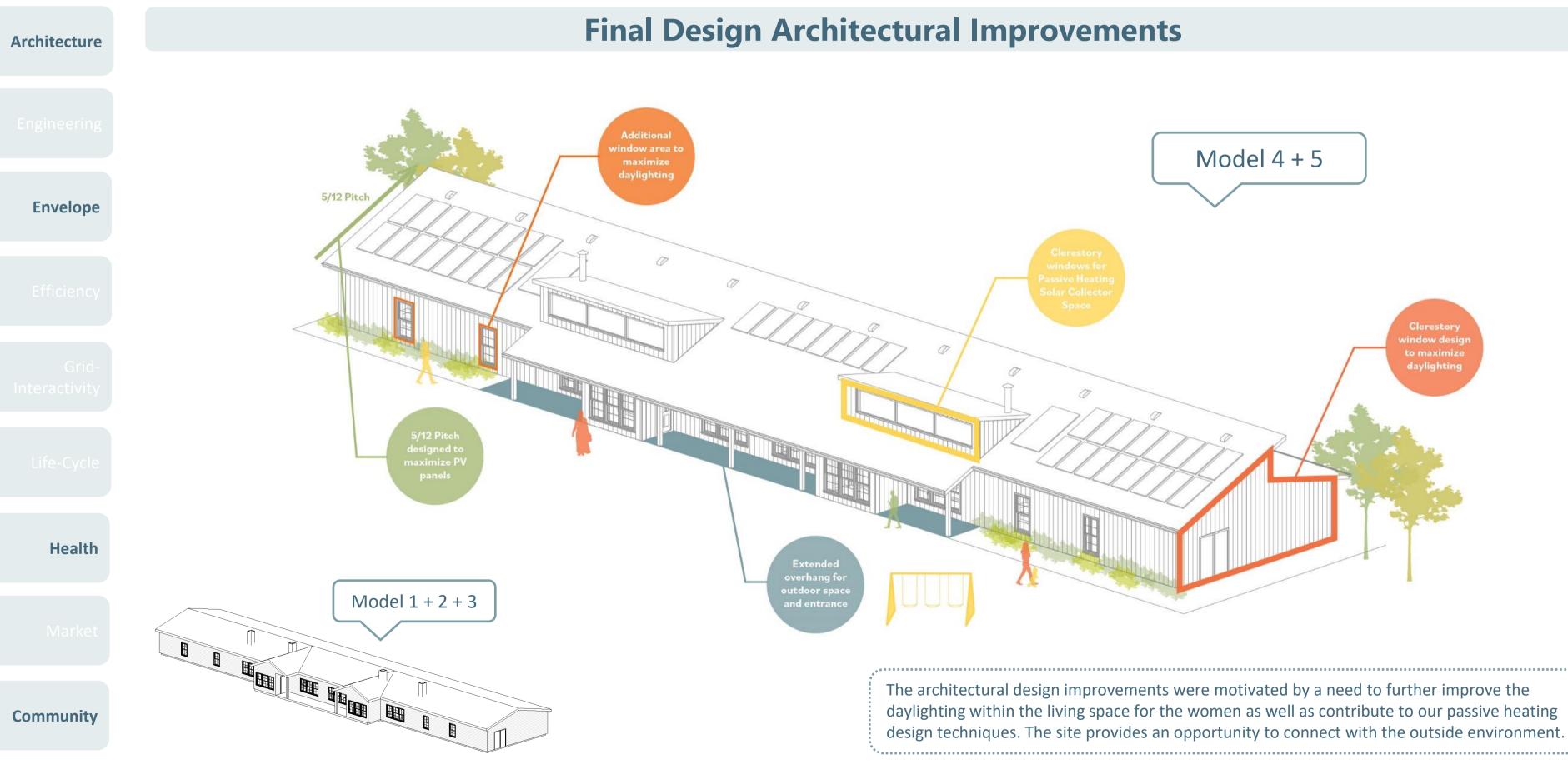
Architecture

Efficiency

Health

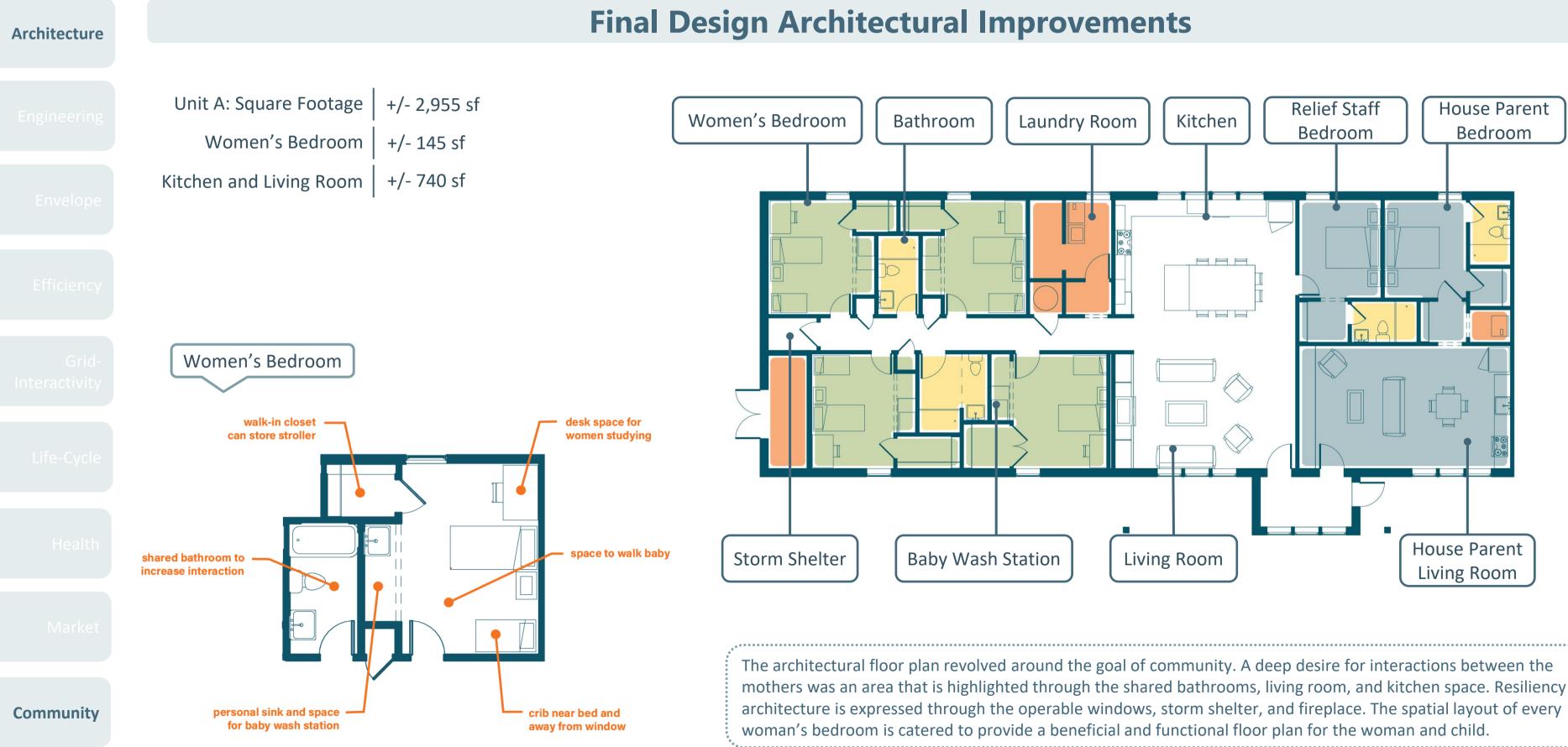


H G R ARCHITECTURE / BUILDING FORM





H C R ARCHITECTURE / FLOOR PLANNING





Architecture

Engineering

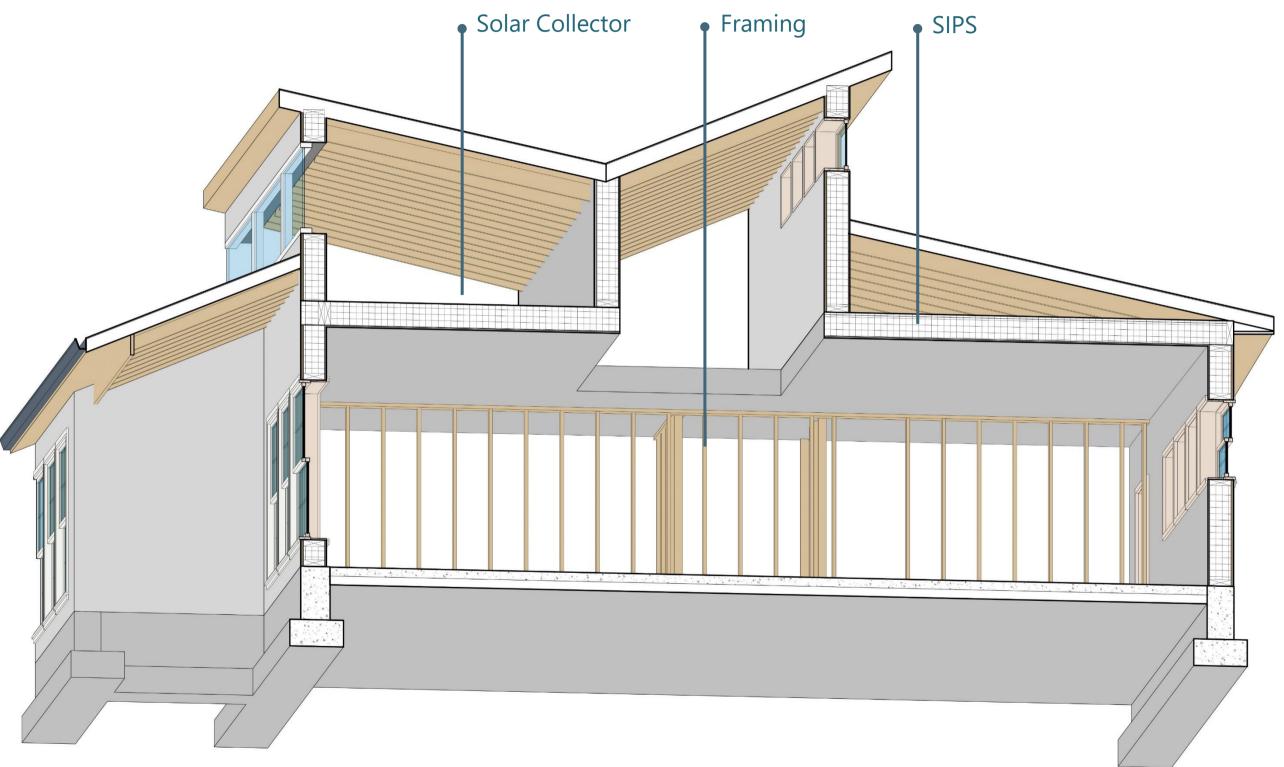
Envelope

BOR ENGINEERING / STRUCTURE

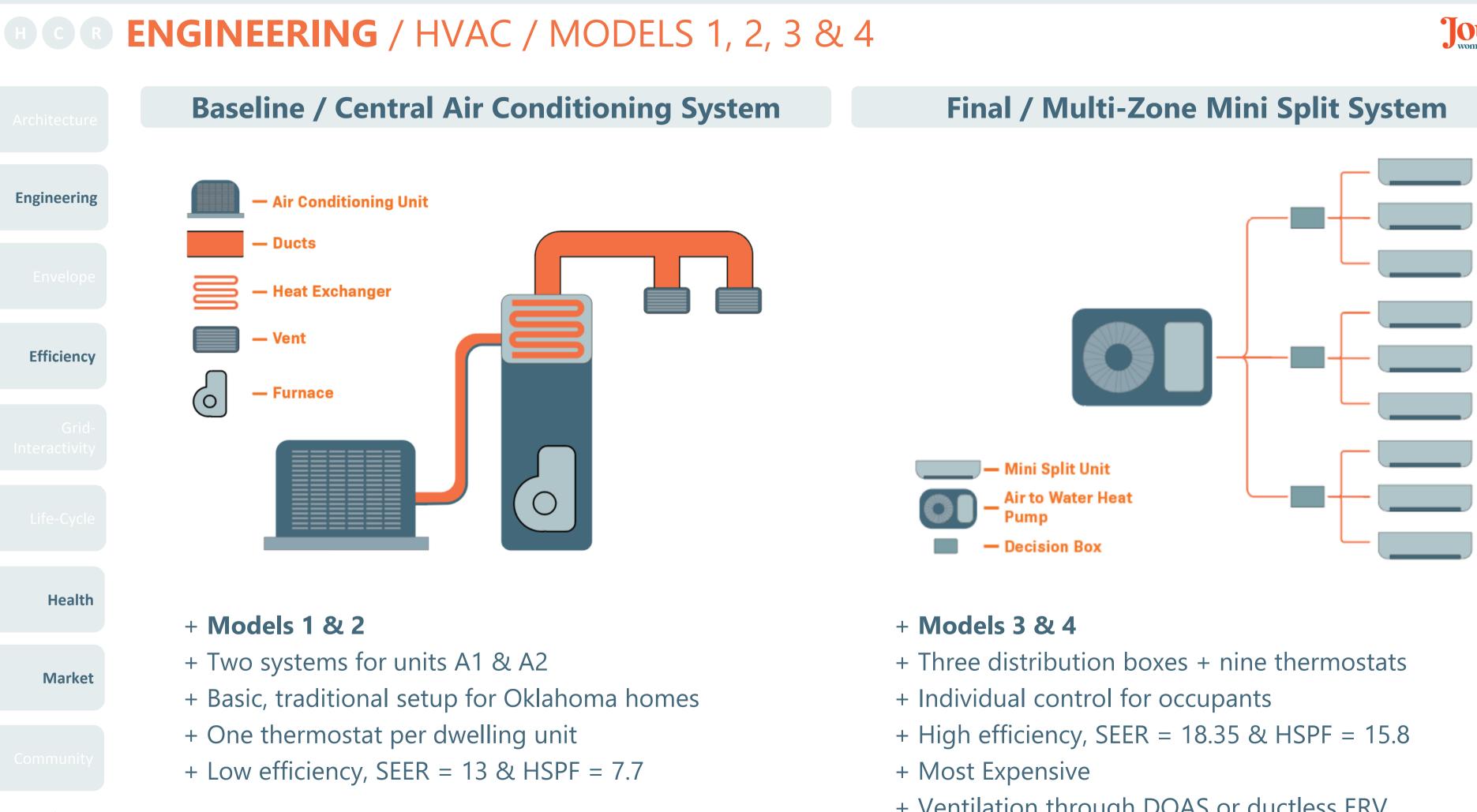
- + Resilient in the wind
 - + Withstands weight of solar heating water tubes/tanks

+ SIPs reduce construction time

- + Reduction in construction waste
- + Slab on grade simplifies construction and provides easy access to the building (using a locally-available low-carbon concrete mix)



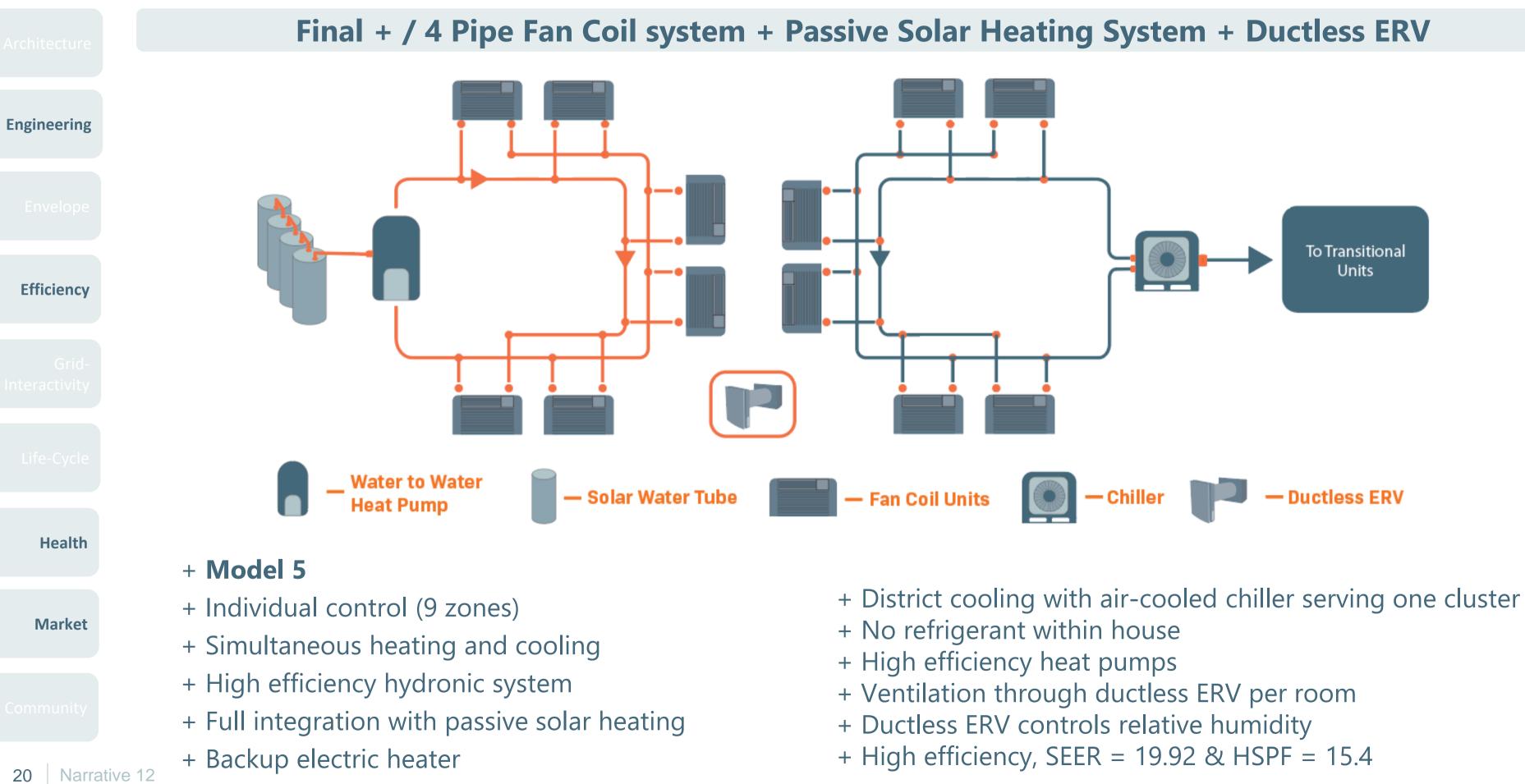






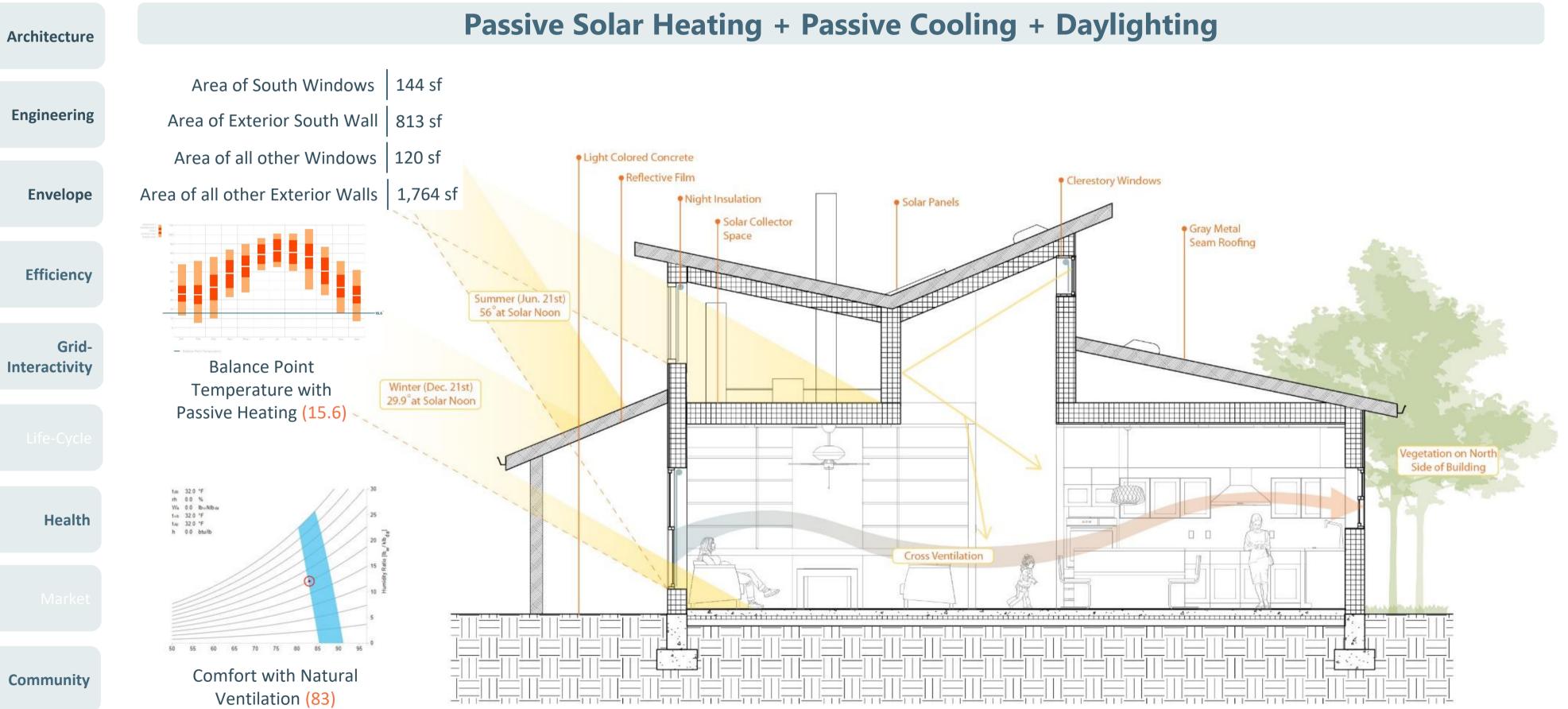
- + Ventilation through DOAS or ductless ERV

B C B ENGINEERING / HVAC / MODEL 5



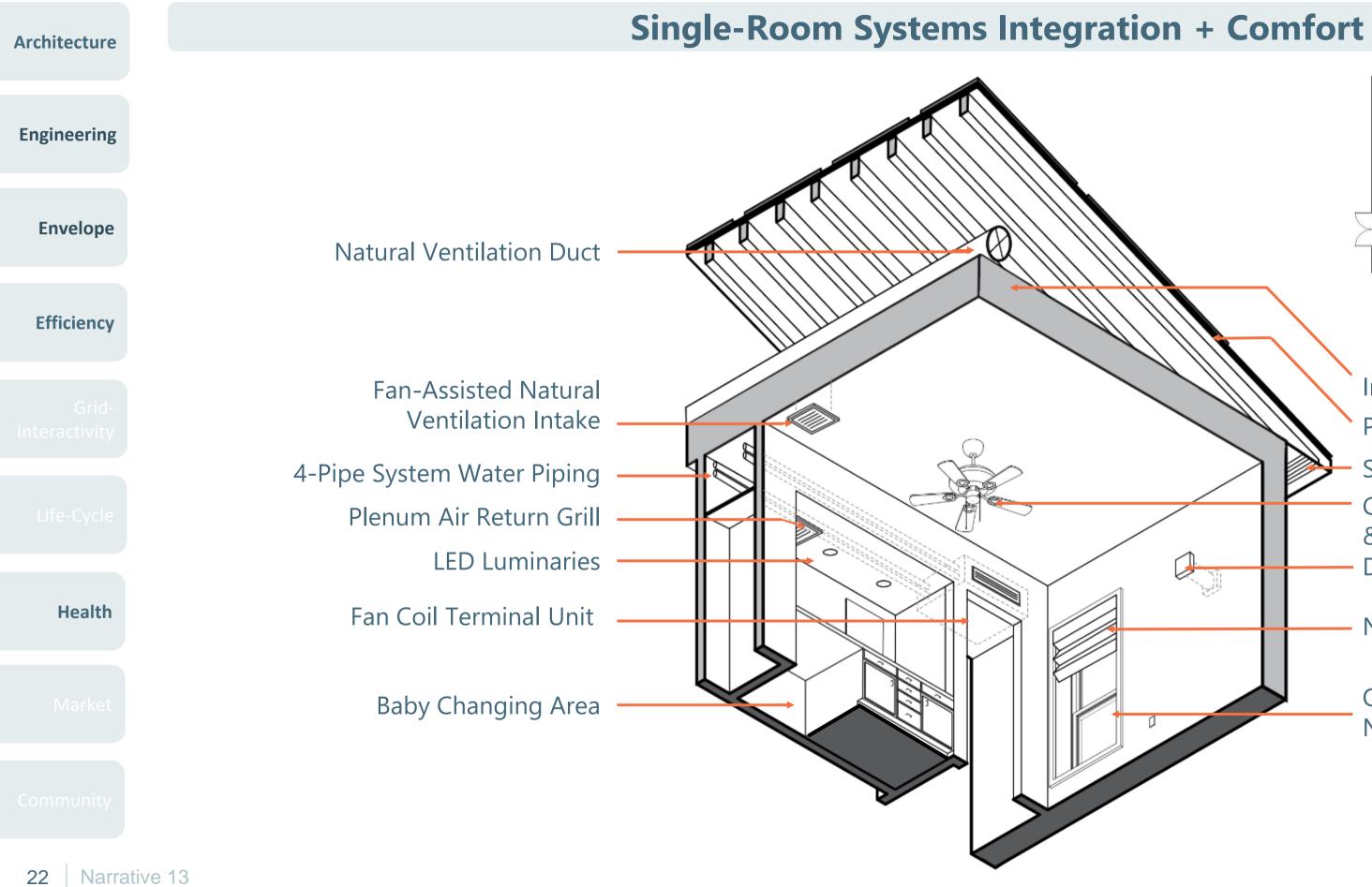


B C R ENGINEERING / PASSIVE SYSTEMS

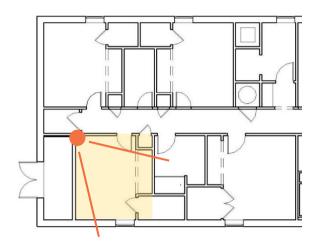




ENGINEERING / SYSTEMS INTEGRATION







Insulated Ceiling (SIPs)

PV Panels

Soffit Vent for the attic

Ceiling Fan for humid hours & natural ventilation Ductless ERV (fresh air inlet)

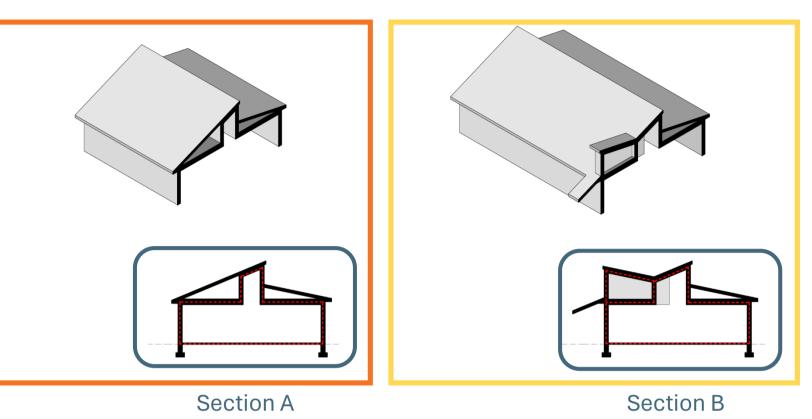
Night Insulation

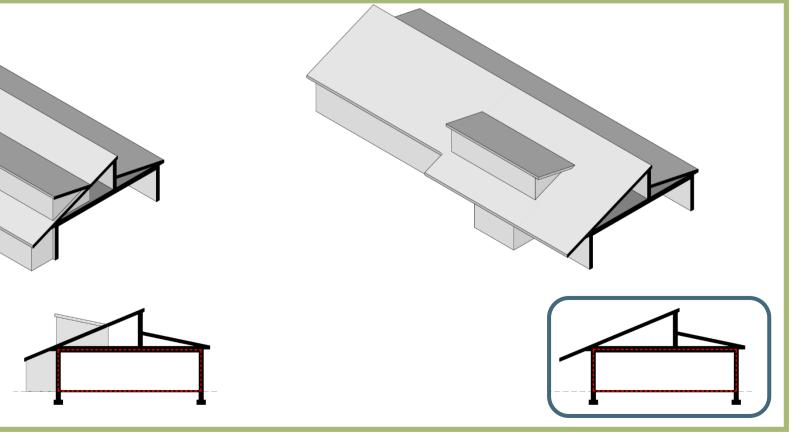
Operable Window Natural Ventilation Inlet

C R ENVELOPE / THERMAL ENCLOSURE

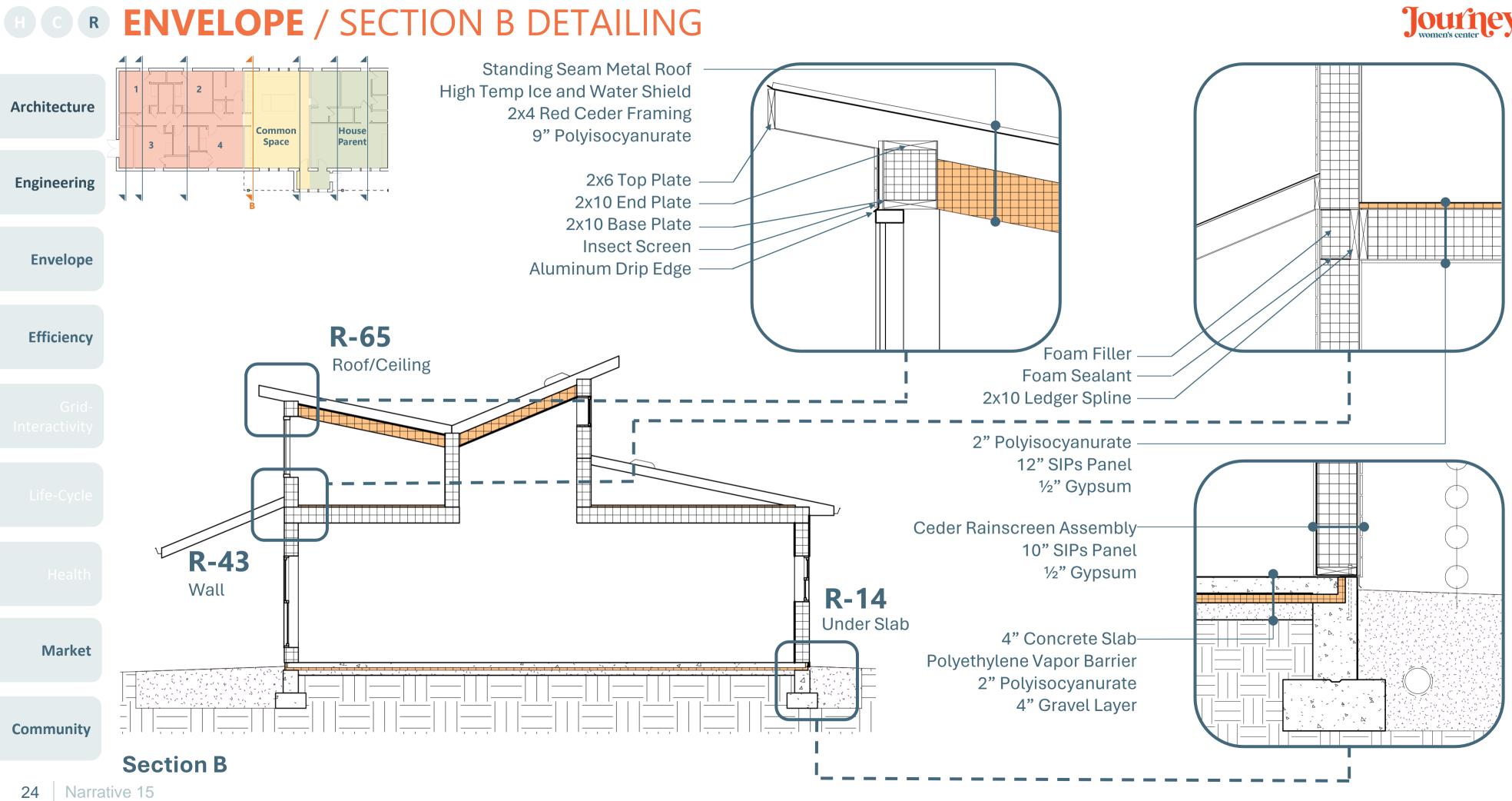




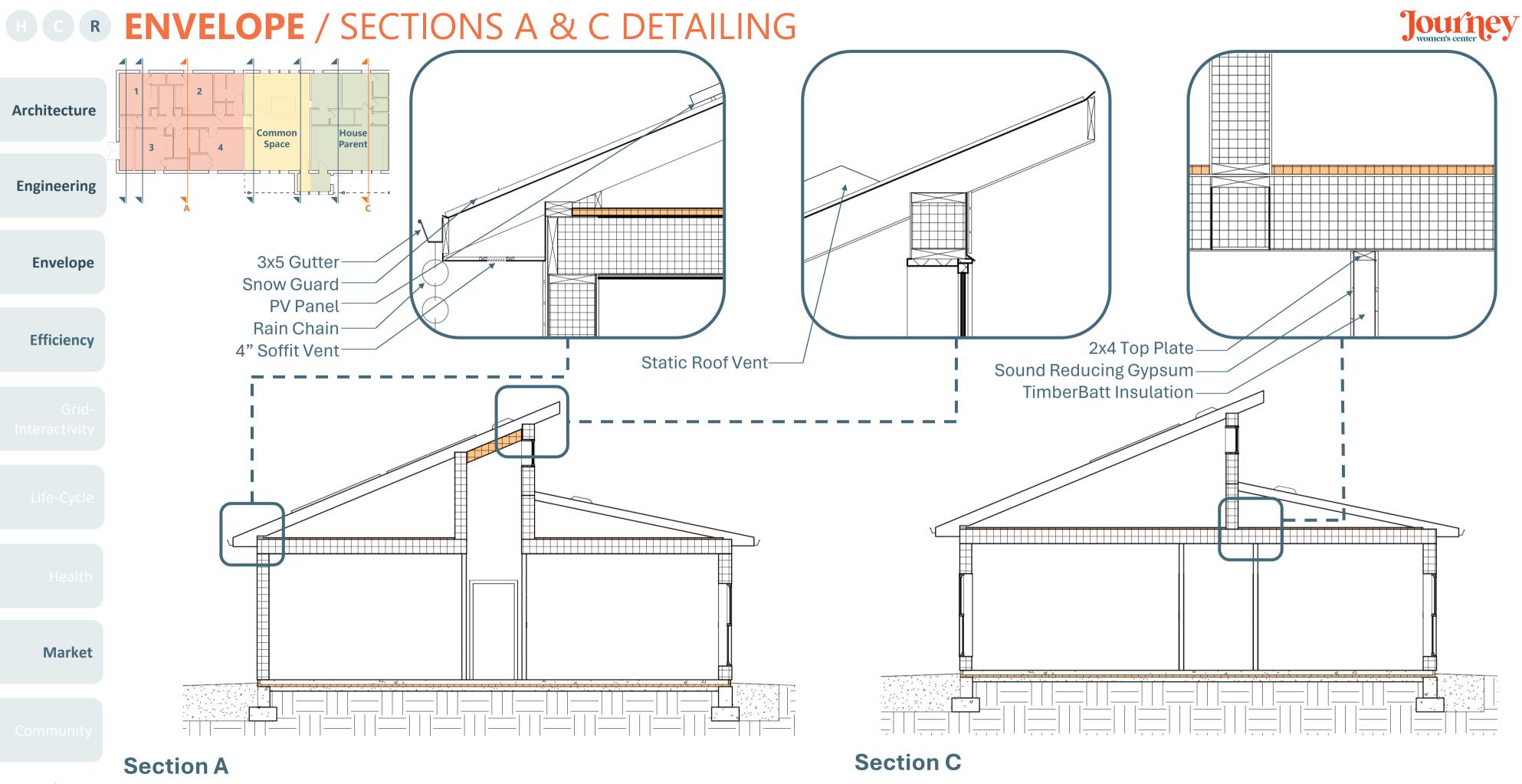




Section C







E C R ENVELOPE / WALL SECTION MODEL



Efficiency

Grid Interactivit

Life-Cycle

Health

Market

Community



Solar Collector



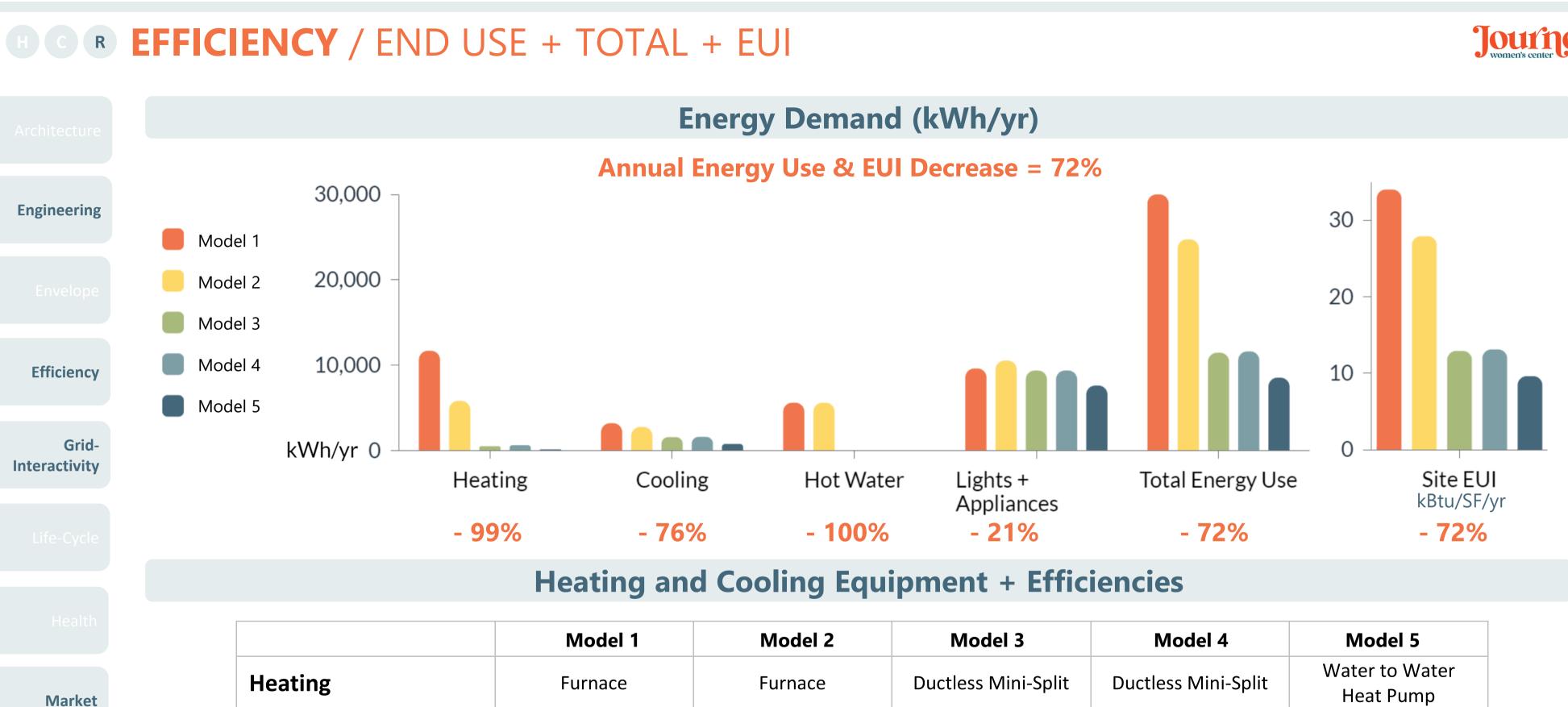
Wall Section







Wall Detailing



9.2

AC Unit

16

Efficiency - HSPF

Efficiency - SEER

Cooling

7.7

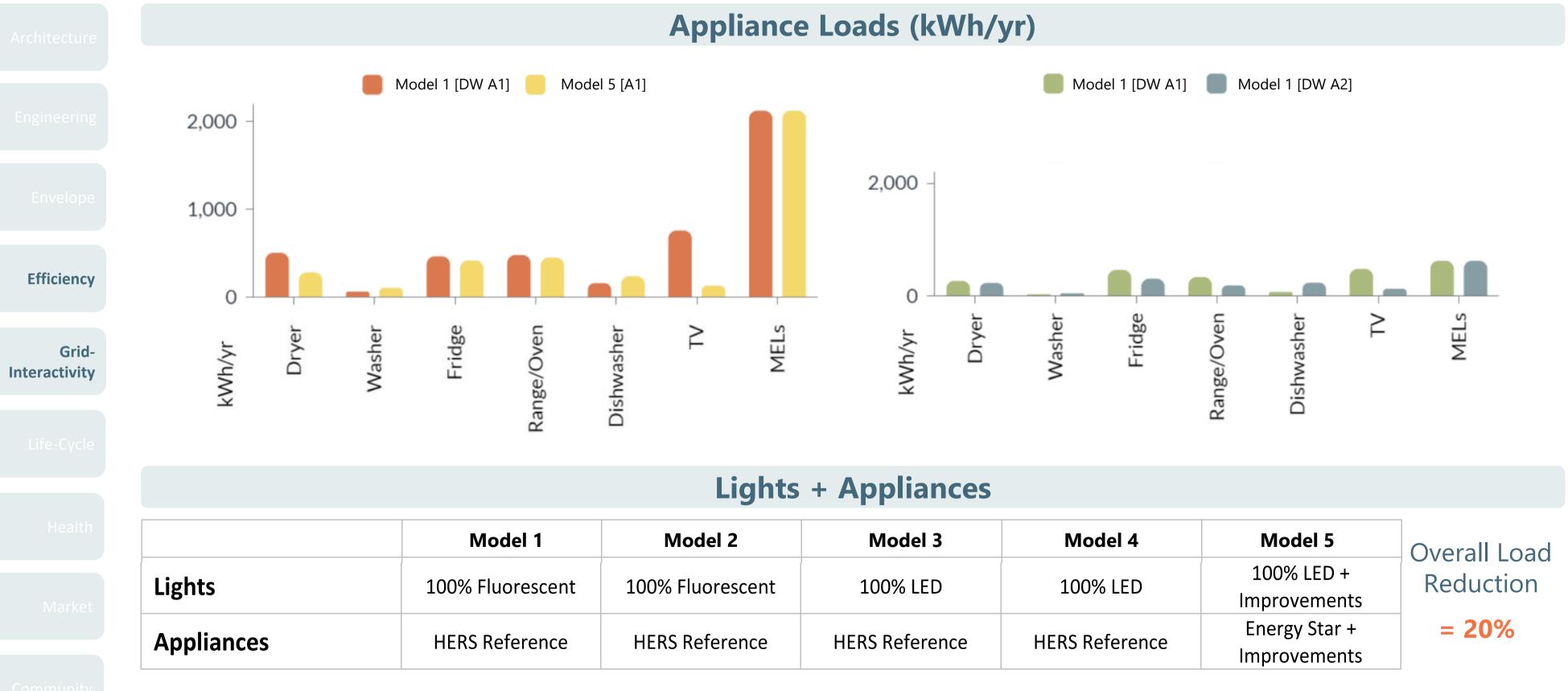
AC Unit

13



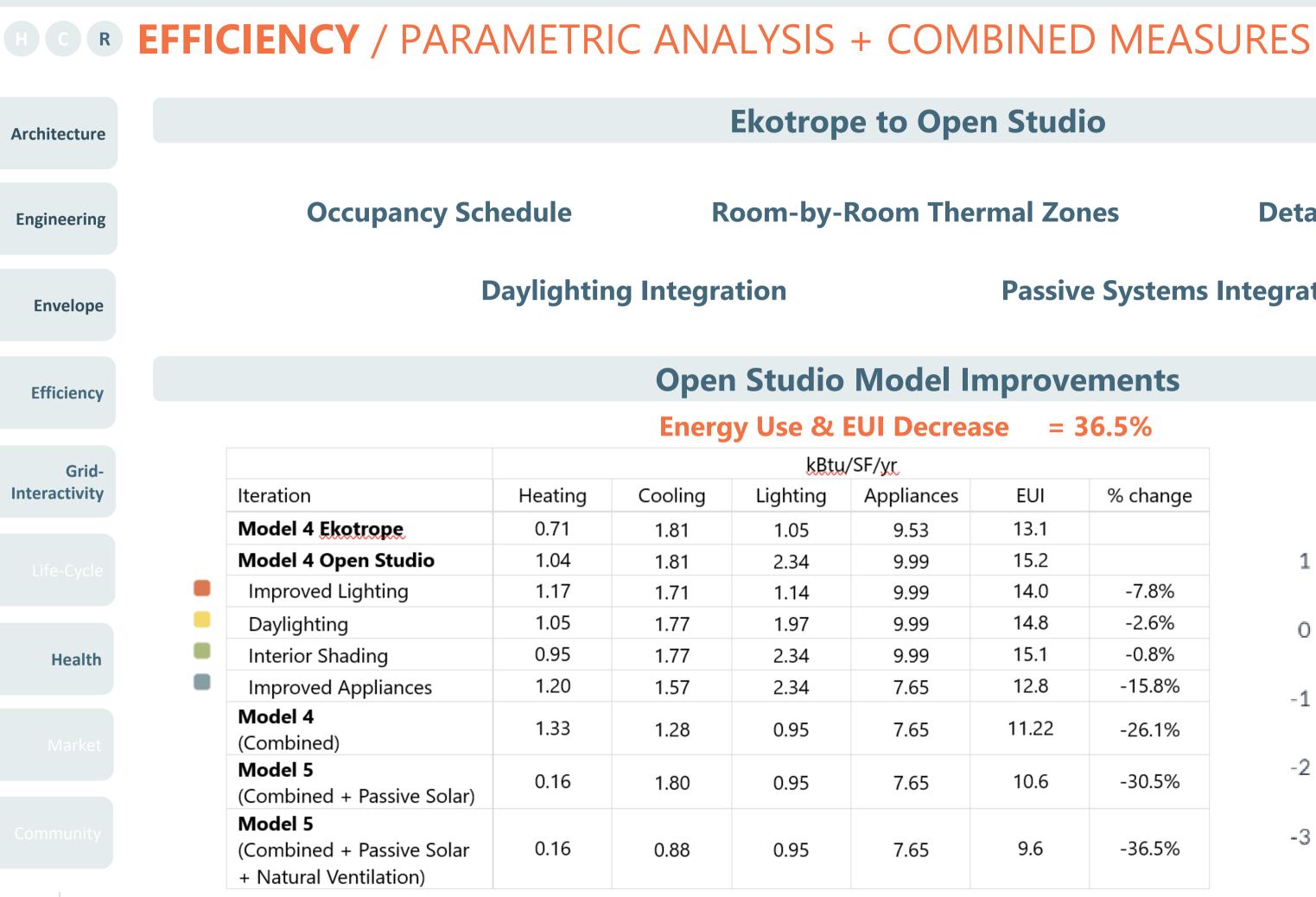
Model 3	Model 4	Model 5	
Ductless Mini-Split	Ductless Mini-Split	Water to Water Heat Pump	
15.8	15.8	15.4	
Ductless Mini-Split	Ouctless Mini-Split Ductless Mini-Split		
18.35	18.35	19.92	

EFFICIENCY / APPLIANCES





	Model 4	Model 5	Overall Load
	100% LED	100% LED + Improvements	Reduction
ce	HERS Reference	Energy Star + Improvements	= 20%





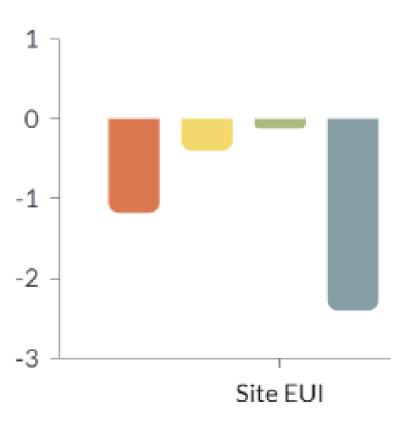
Detailed Hourly Outputs

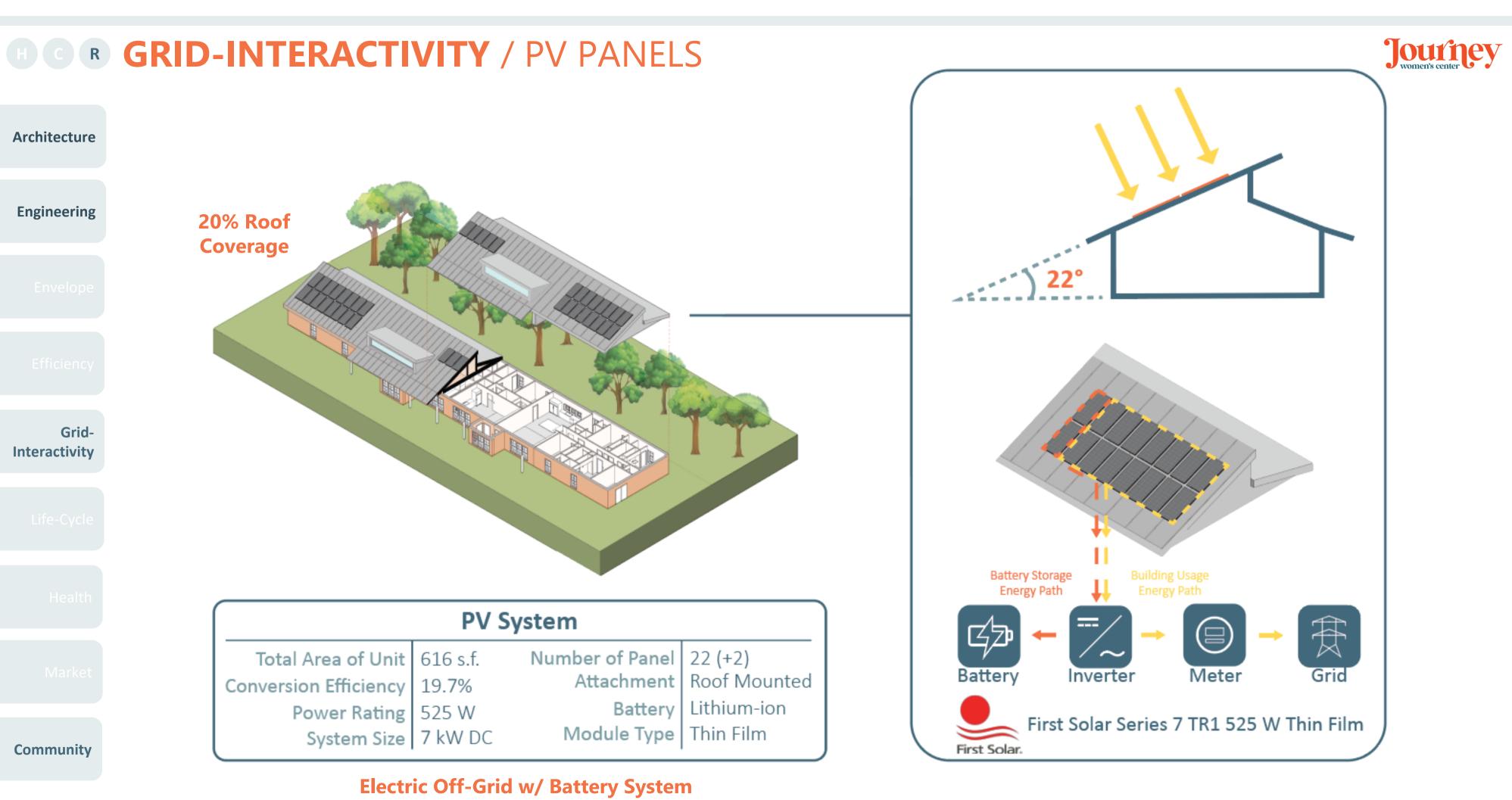
Passive Systems Integration

= 36.5%

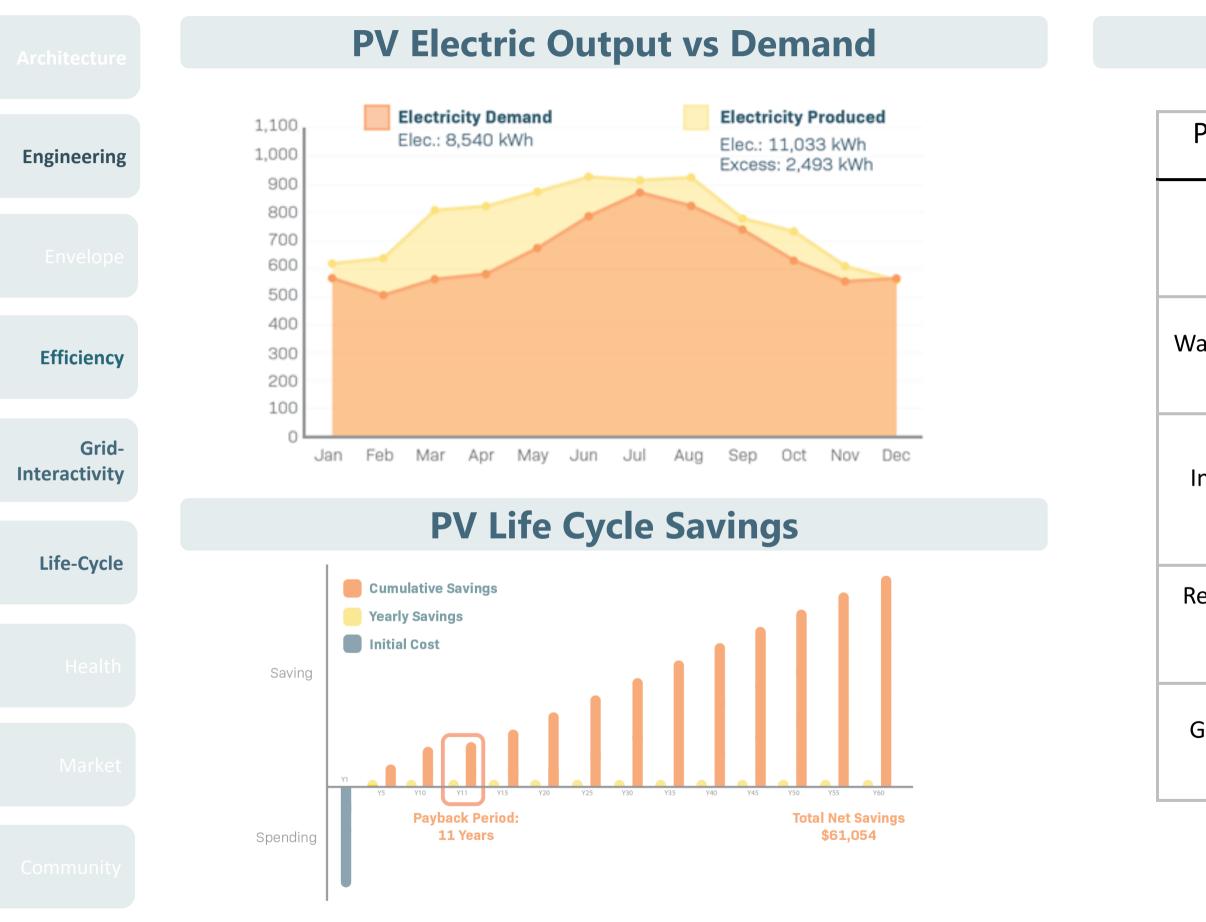
JI	% change
8.1	
5.2	
l.0	-7.8%
.8	-2.6%
5.1	-0.8%
2.8	-15.8%
.22	-26.1%
).6	-30.5%
.6	-36.5%

EUI Decrease from Model 4 Open Studio





GRID-INTERACTIVITY



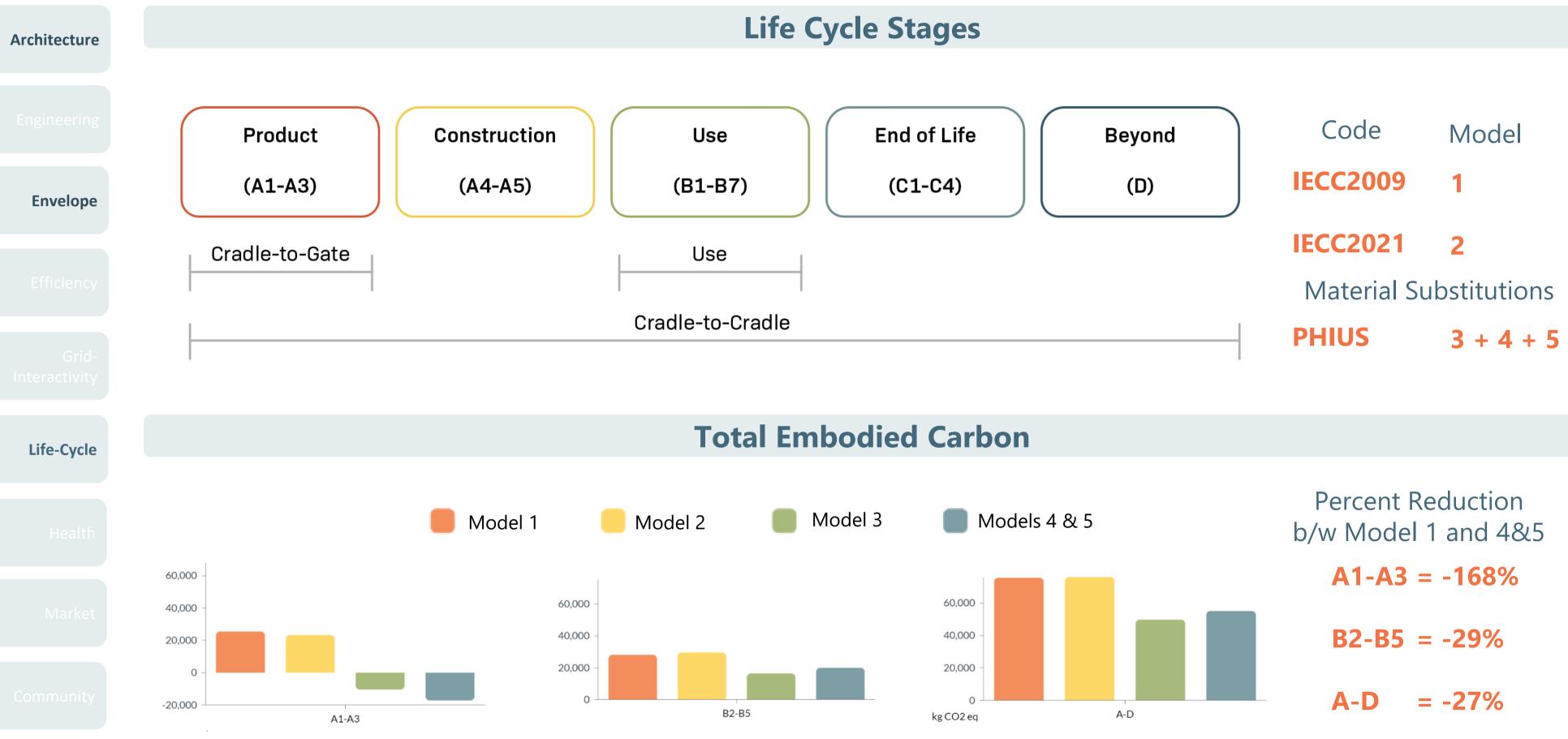


PV Panel Carbon

PV Panel Em	bodied CO ₂	Grid Emissions		
LCA A-D	0.258	SPSO Emission	138	
	kg CO ₂ eq/W	Factor	kg CO ₂ /MBtu	
'attage/Panel	525 W	SPSO Emission	0.4701	
allage/ Fallel	525 VV	Factor	kg CO₂/kWh	
		Final +		
Initial Panel	22	Energy Demand	8,540 kWh/yr	
eplacement	2	GWP/yr	4,015	
Panels	ζ.	Gvvi/yi	kg CO₂ eq	
GWP/60 yrs	3,251	GWP/60 yrs	240,881	
	kg CO2 eq		kg CO₂ eq	

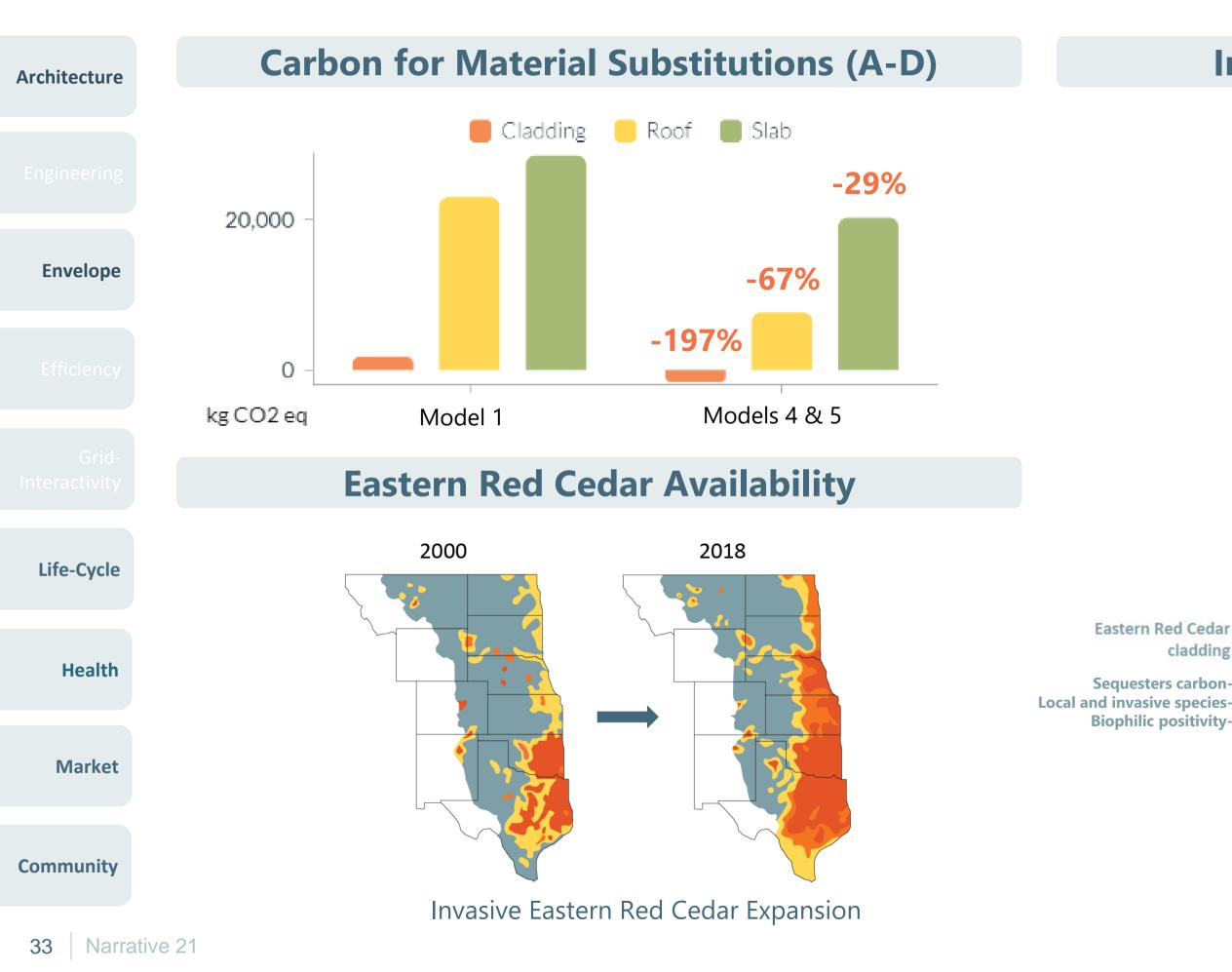
PV vs Grid Only Electricity = -99%

I C R LIFE-CYCLE / EMBODIED CARBON / SUMMARY



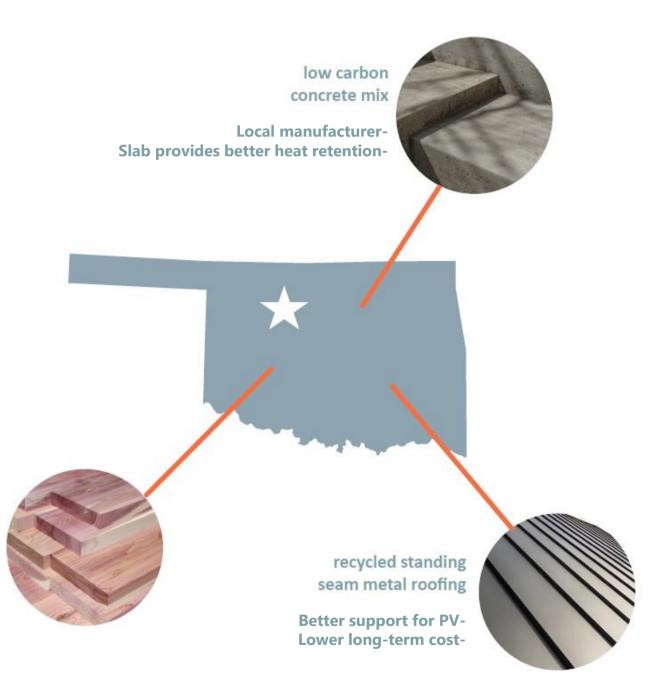


B C R LIFE-CYCLE / EMBODIED CARBON / MATERIALS





Improved Materials & Location



BOR LIFE-CYCLE / MATERIAL MODEL









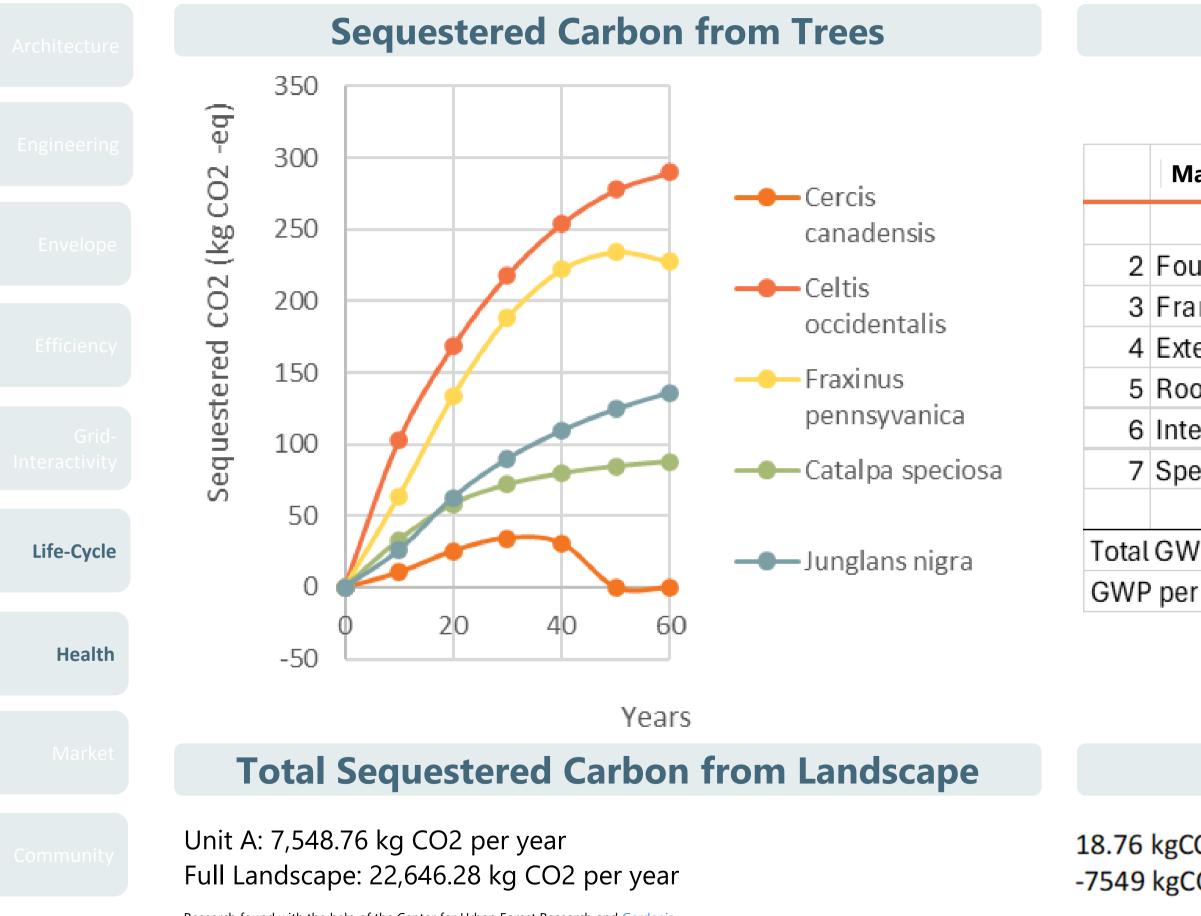


Front View + Entry Detail



Back View + Corner Detail

C R LIFE-CYCLE / EMBODIED CARBON / LANDSCAPING



Research found with the help of the Center for Urban Forest Research and Gardenia





Carbon by Building Category

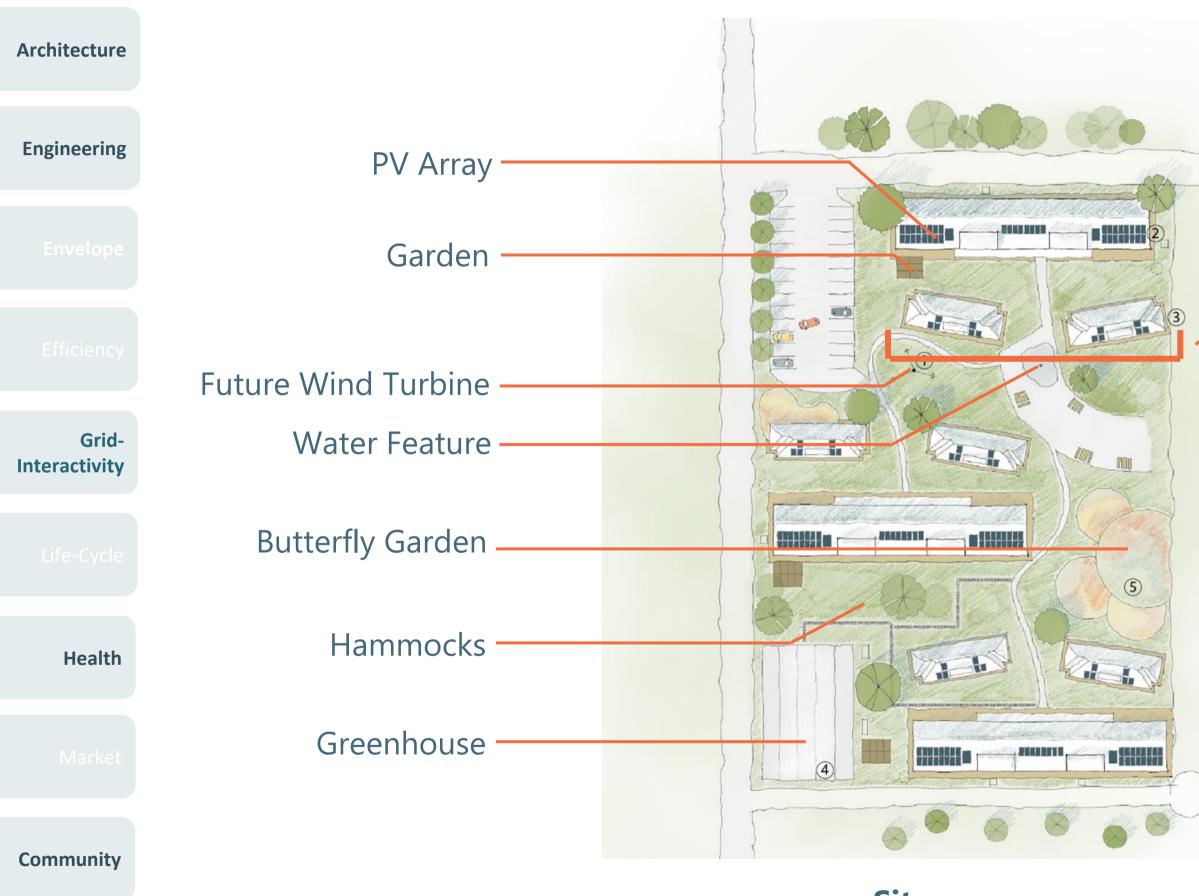
laterials	Model 1	Models 4 & 5	
undation	29,767	20,293	
aming	-2,081	-14,319	
terior Walls	7,645	14,677	
ofing + Ceiling	25,210	19,018	
eriors	9,137	16,832	
ecialties	219	165	
VP	69897	56666	
er SF	23.14	18.76	

Net Carbon Cradle-to-Cradle

18.76 kgCO2/SF / 60 yrs = 0.31 kgCO2/SF/yr -7549 kgCO2/yr / 3021 SF = -2.5 kgCO2/SF/yr = -2.19 kg CO2 eq/SF/yr

86% more carbon sequestered than produced

H C R HEALTH / EXTERIOR



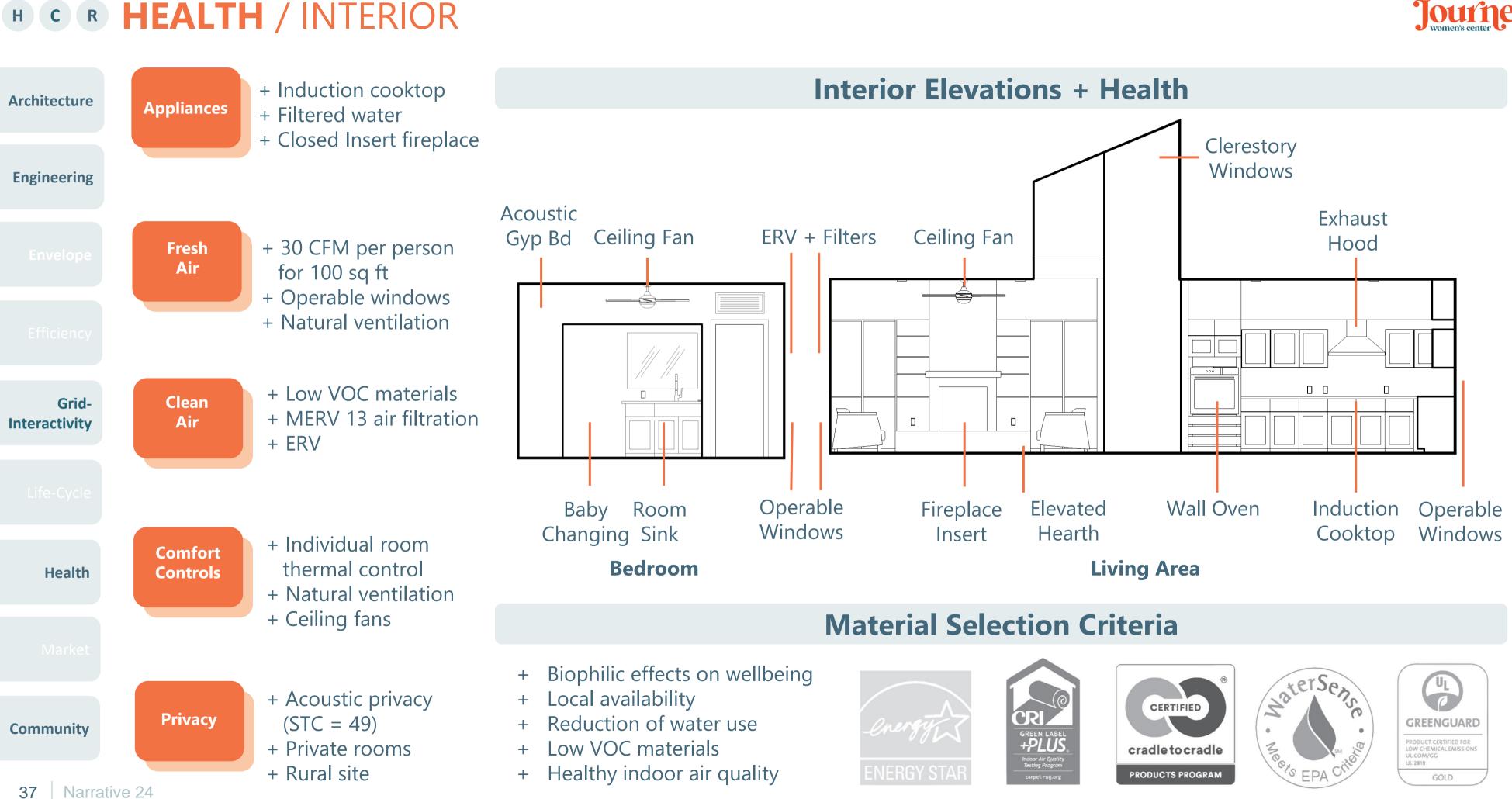
Site





Bioswale

The incorporation of biophilic design elements within the site aims to cultivate a sense of tranquility and connection with nature for its occupants. Biophilic design fosters a safe and nurturing environment. The design concept prioritizes organic elements that facilitate both communal gatherings and solitary moments of reflection. The bioswale on the north side of the site serves dual purposes by creating gathering spaces and harvesting rainwater.





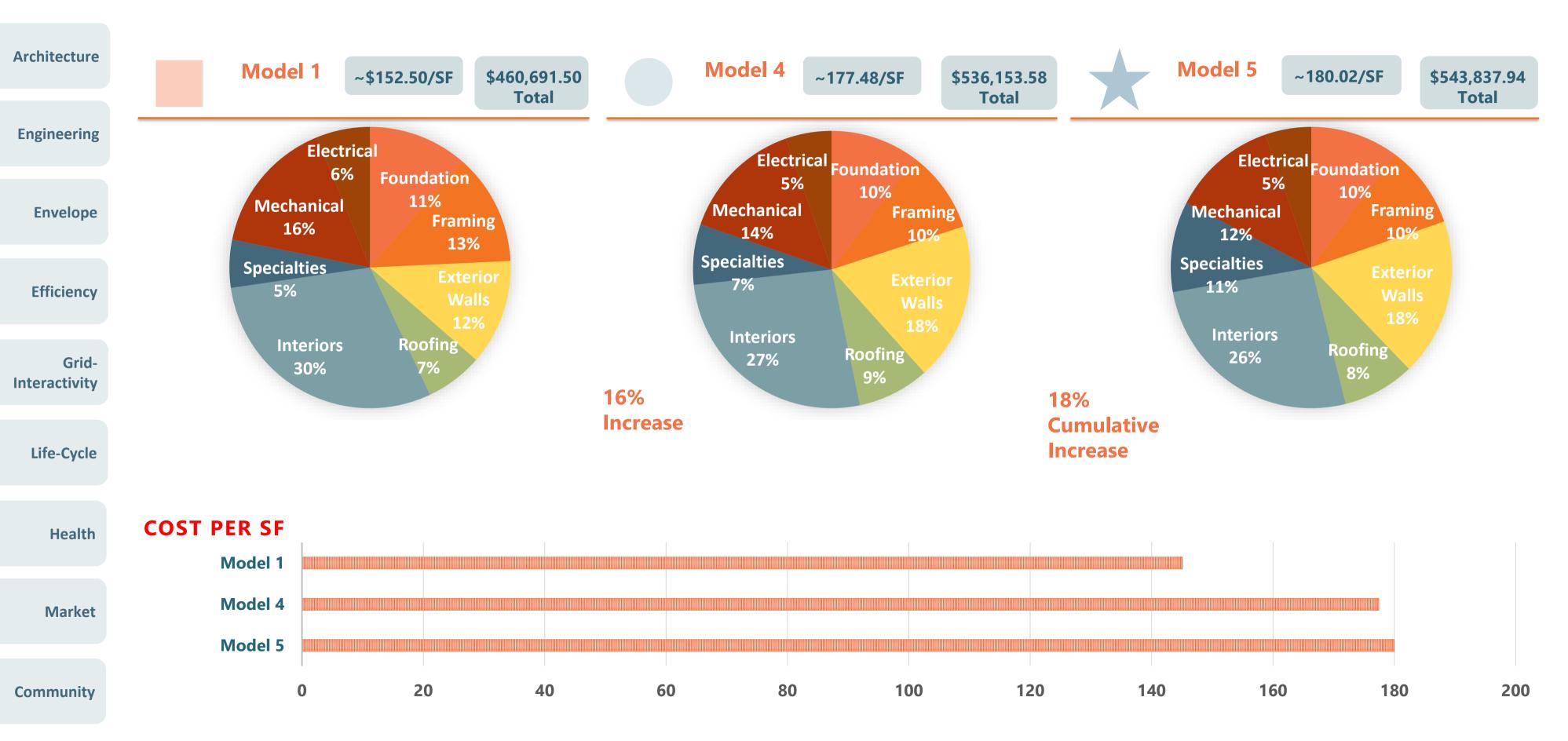
B C R MARKET / COST ESTIMATION

Architecture							
	Building Information	Мос	del 1	Мо	del 4	Mod	lel 5
Engineering		Total Cost (\$)	Replacement	Total Cost (\$)	Replacement	Total Cost (\$)	Replacement
	2 Foundation	\$37,456.60	\$0.00	\$39,365.28	\$0.00	\$39,365.28	\$0.00
Envelope	3 Framing	\$42,365.22	\$0.00	\$37,133.95	\$0.00	\$37,133.95	\$0.00
	4 Exterior Walls	\$39,950.16	\$37,306.32	\$70,332.37	\$59,114.96	\$70,332.37	\$59,114.96
E 60:	5 Roofing + Ceiling	\$21,690.78	\$35,859.27	\$32,116.07	\$23,985.77	\$32,116.07	\$23,985.77
Efficiency	6 Interiors	\$97,690.30	\$120,113.97	\$101,491.14	\$123,104.59	\$101,491.14	\$123,104.59
	7 Specialties	\$18,130.11	\$0.00	\$27,018.73	\$15,852.90	\$41,234.05	\$15,852.90
Grid-	8 Mechanical	\$51,488.87	\$0.00	\$55,043.68	\$0.00	\$46,991.81	\$0.00
Interactivity	9 Electrical	\$20,293.32	\$48,292.45	\$20,465.62	\$49,153.95	\$20,656.45	\$49,153.95
	Subtotal	\$329,065.36	\$241,572.01	\$382,966.84	\$271,212.17	\$389,321.12	\$271,212.17
Life-Cycle	Contractor Fees (General Conditions, Overhead, Profit)	\$131,626.14	\$96,628.80	\$153,186.74	\$108,484.87	\$155,728.45	\$108,484.87
	Architectural Fees	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00
	User Fees	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00	\$0.00
Health	Total	\$460,691.50	\$338,200.81	\$536,153.58	\$379,697.04	\$545,049.57	\$379,697.04
	Cost Per SF	\$152.50		\$177.48		\$180.42	
Market	Total Life Span Cost		\$798,892.32		\$915,850.61		\$924,746.61

Community

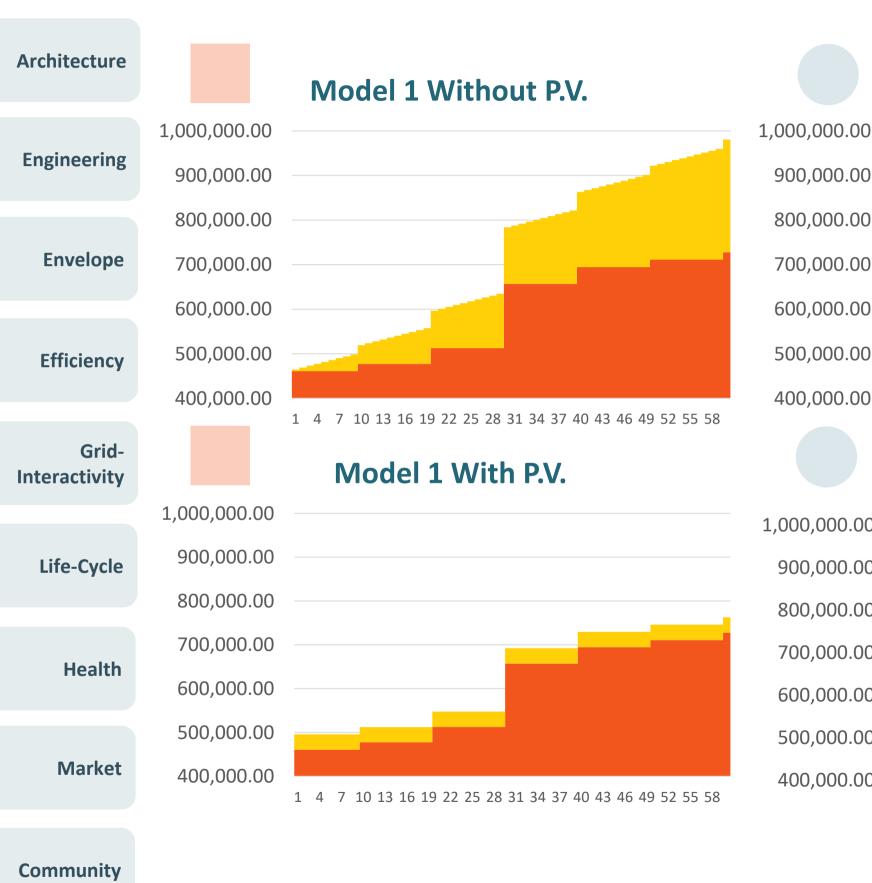


B C R MARKET / COST ESTIMATION

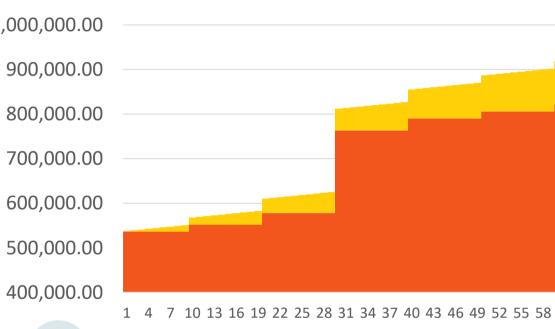




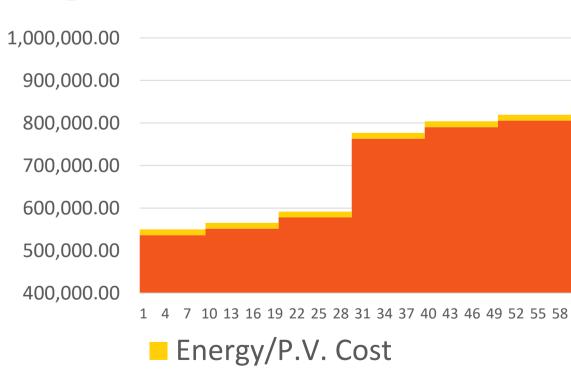
B C R MARKET / LCA / CUMULATIVE COST



Model 4 Without P.V.



Model 4 With P.V.



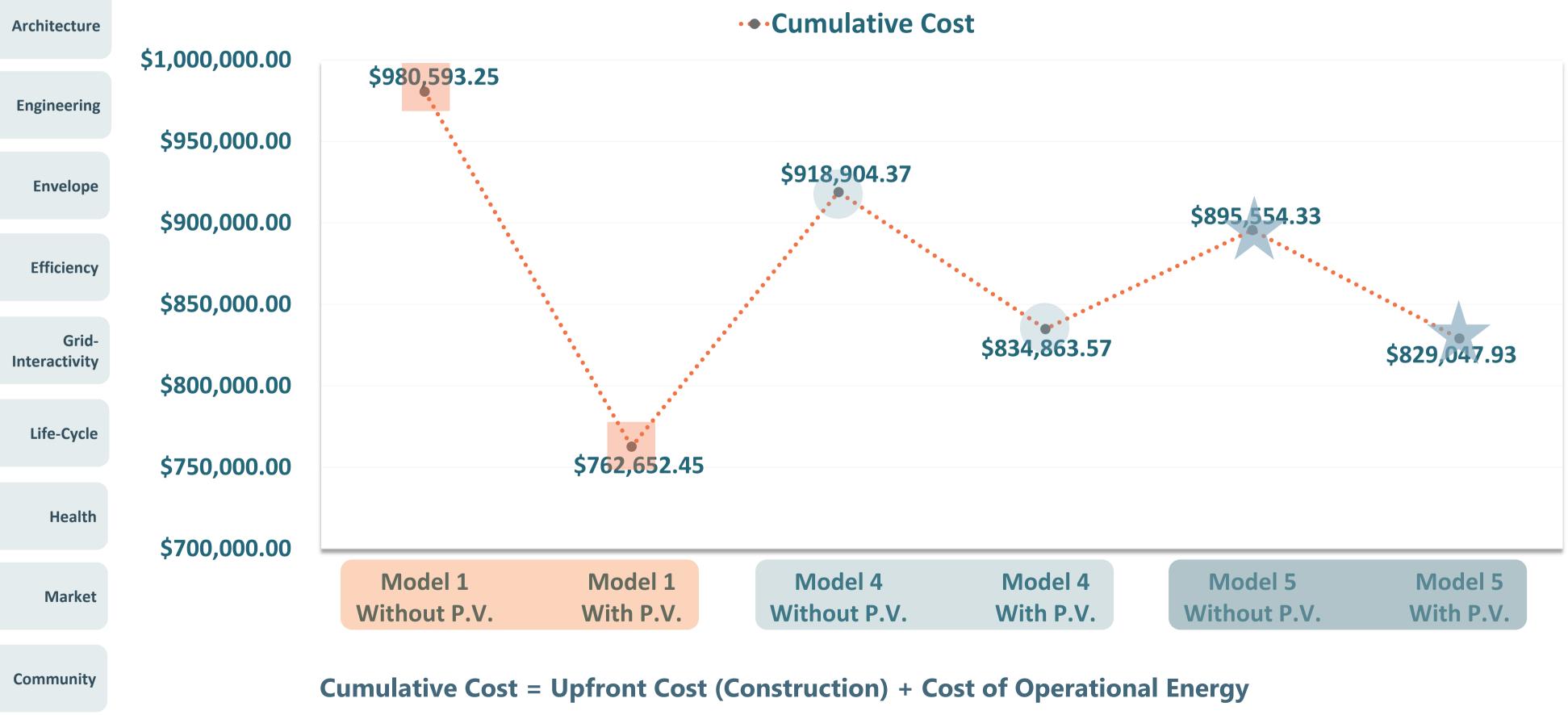
Building and Material Replacement Cost





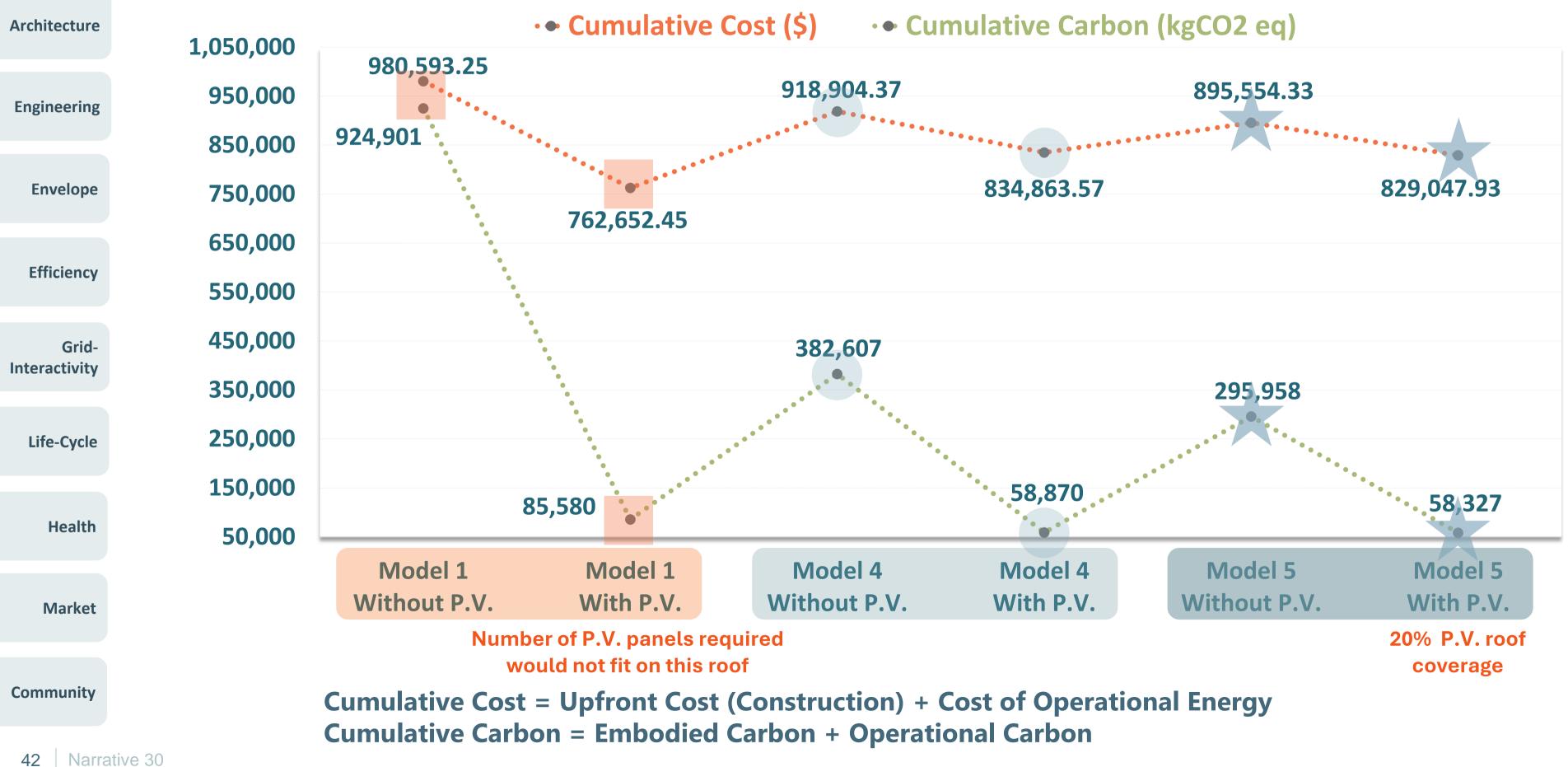
al

Image: Image:





MARKET / LCA / ENERGY + COST + CARBON







Narrative 31 43



C COMMUNITY / SITE MODEL







Site Axon





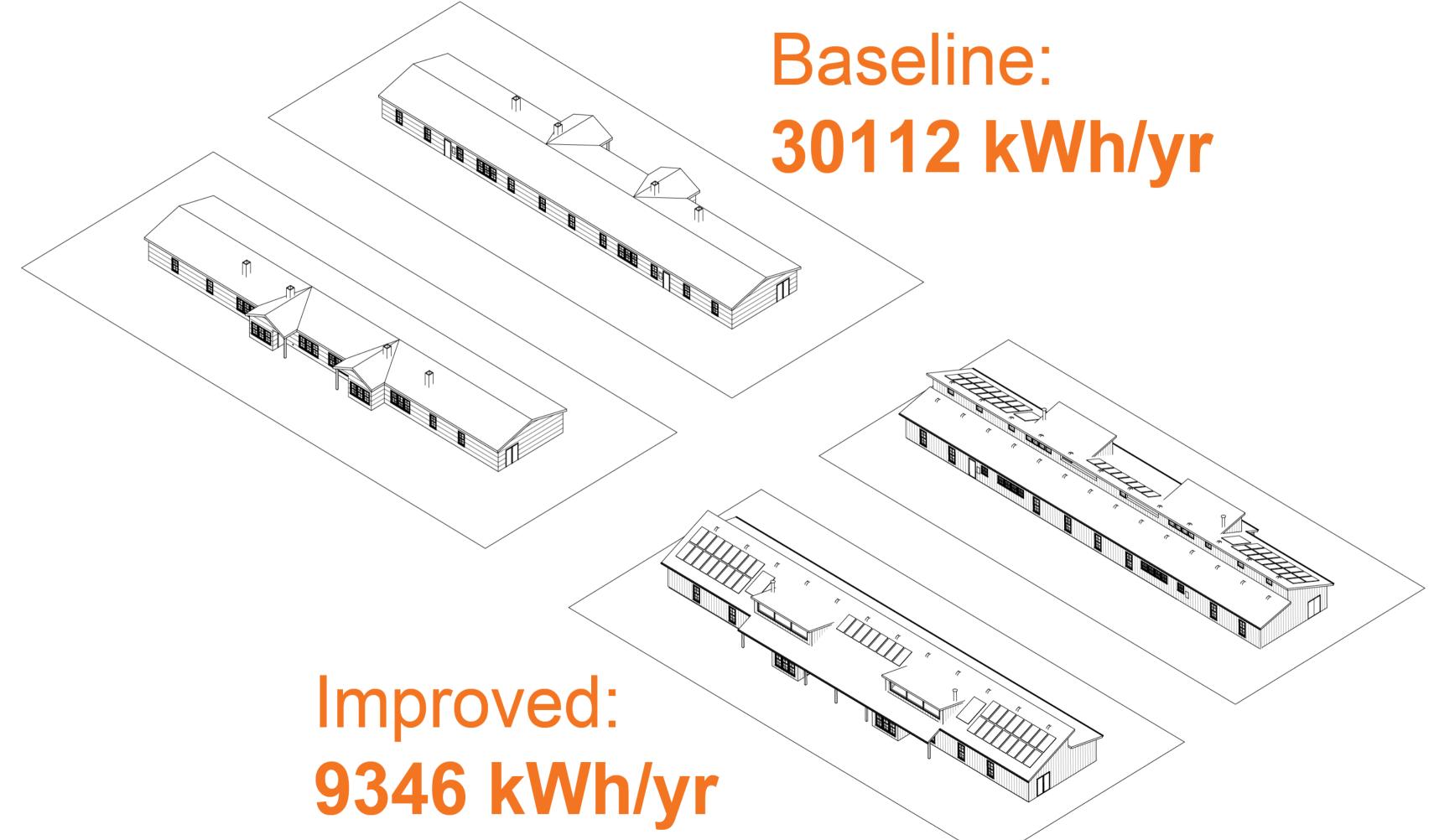
Community Resiliency Hope



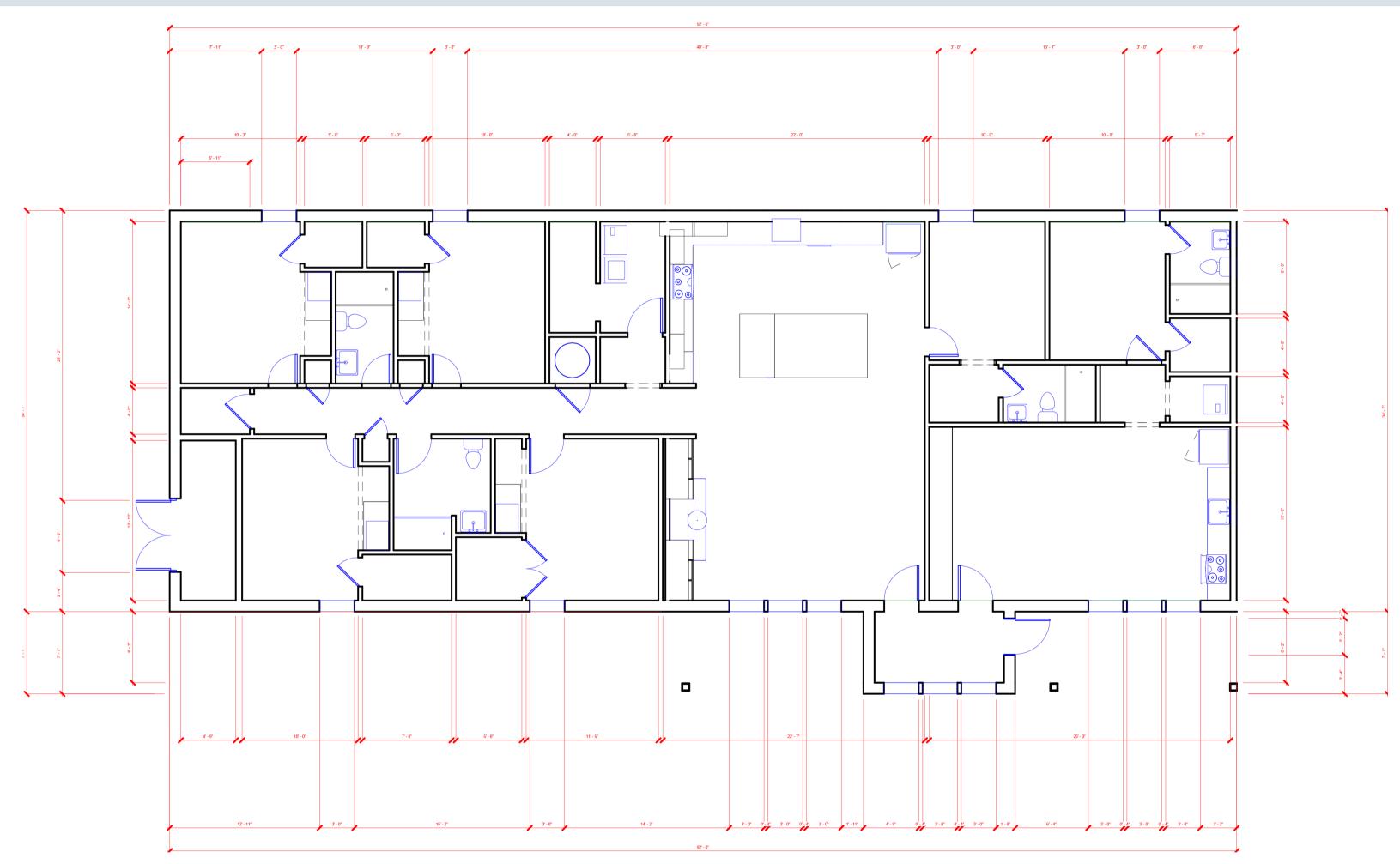
THANK YOU! QUESTIONS?



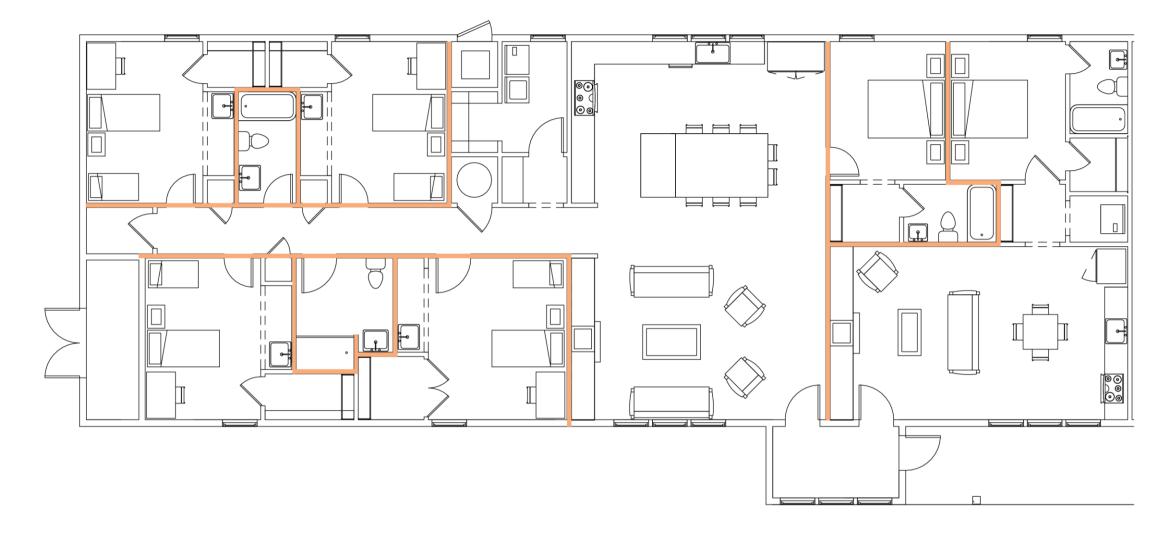
Model 1 vs. Model 5 Comparison



Dimensioned Plan, Units A1 & A2



Acoustic Partitions Plan, Units A1 & A2



STC Rating of 49

International Well Building Institute recommends a minimum STC rating of 40 between circulation zones and regularly occupied spaces.



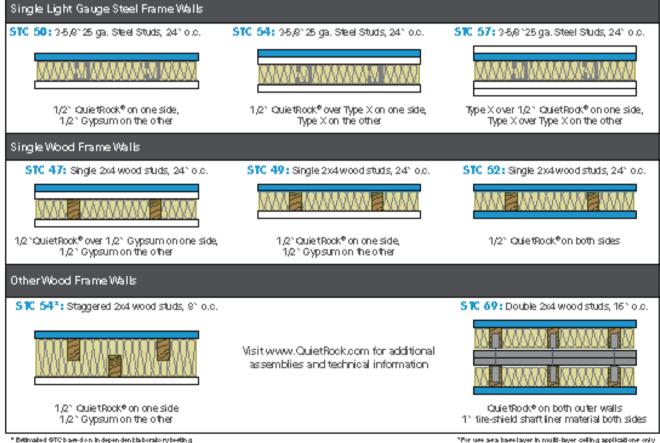
Product Specifications:

Thickness: 1/2" (12.7mm), tapered edges Width: 4' (1220mm) 8' (2438mm), 9' (2743mm), 10' (3048mm), Lengths: 121(3658mm) Weight: 2.13 lbs/sqft STC-rated Assemblies (per ASTM E 90): 47-52 Flame Spread (per AST M E 64): Class A Product Standards: C1766 Installation Standards: ASTMIC 840; GA-214, GA-216

UL Assembly: 🕥

QuietRock® 510 is approved for use as an additional layer on one or both sides of the U300, U400, V400 and W400 wall designs as the face layer or attached to the studs. QuietRock® 510 is approved for use as an additional layer in the L500 and M500 series floor/ceiling assemblies.¹ QuietRock® 510 panel not evaluated nor intended as a substitute for the required layer(s) of UL Classified Gypsum Board in the above listed designs.

Common Wall Assemblies:



Betimabed GTC base don in dependen bisboratory beeting

The information contained in this do ament lefting eneral purposes only. Polares and specifications are subject to change. The diagrametand stated STC rating state intended to encurs a signific. Construction practices have an information of the walk and construction methods factor in effective exand control. By a state of the source to example, the integrity of the walk and construction methods factor in effective exand control. By a state of the source to example, the integrity of the walk and construction methods factor in effective exand control. By a state of the source to example, the integrity of the walk and construction methods factor in effective exand in effective and states of 122P (2000) or more whould be avoid to example to be or of the basis of the source on supported if energies product. Proper care should be about the integrity of the source on exported in the source on exported in a dry an effective example.



PABCO® Gypsum (3735). Cherry Street, Newark, CA 34550 (1.800.7978159) www.Pateo5ypsum.com (www.CuietRock.com (PN: 101.00017-0214)8 9 ST3 PNBCO[®] Opport. SI highlar interved. PSECO[®] Opport. the PSECO[®] logo. ELEVRE[®], OuteR., Out

Floor Plan, Units A1 & A2





Sherwin Williams – Pure White ProMar 200 Zero

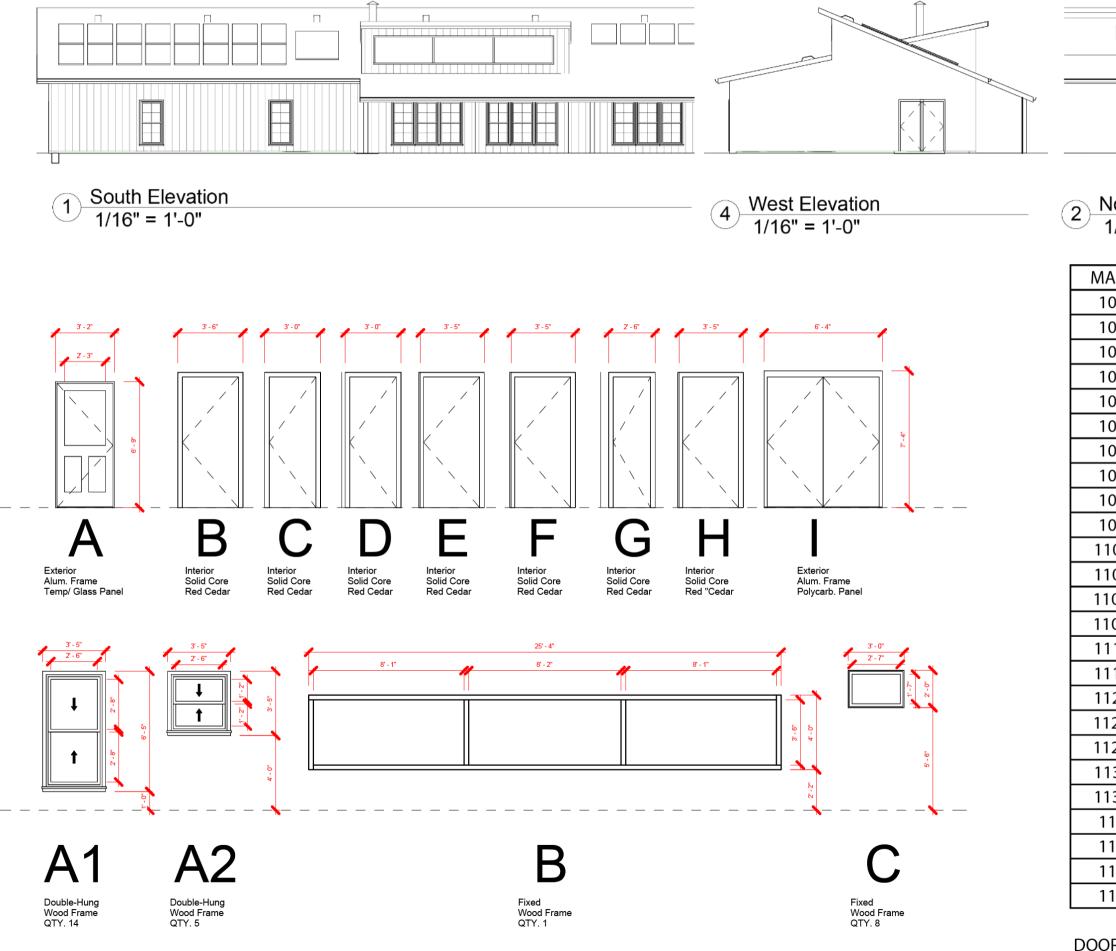


ShawContract - Reside 12 MIL Hearth 9141



Local Lumber Eastern Red Cedar Wood

Door and Window Schedules





North Elevation

1/16" = 1'-0"

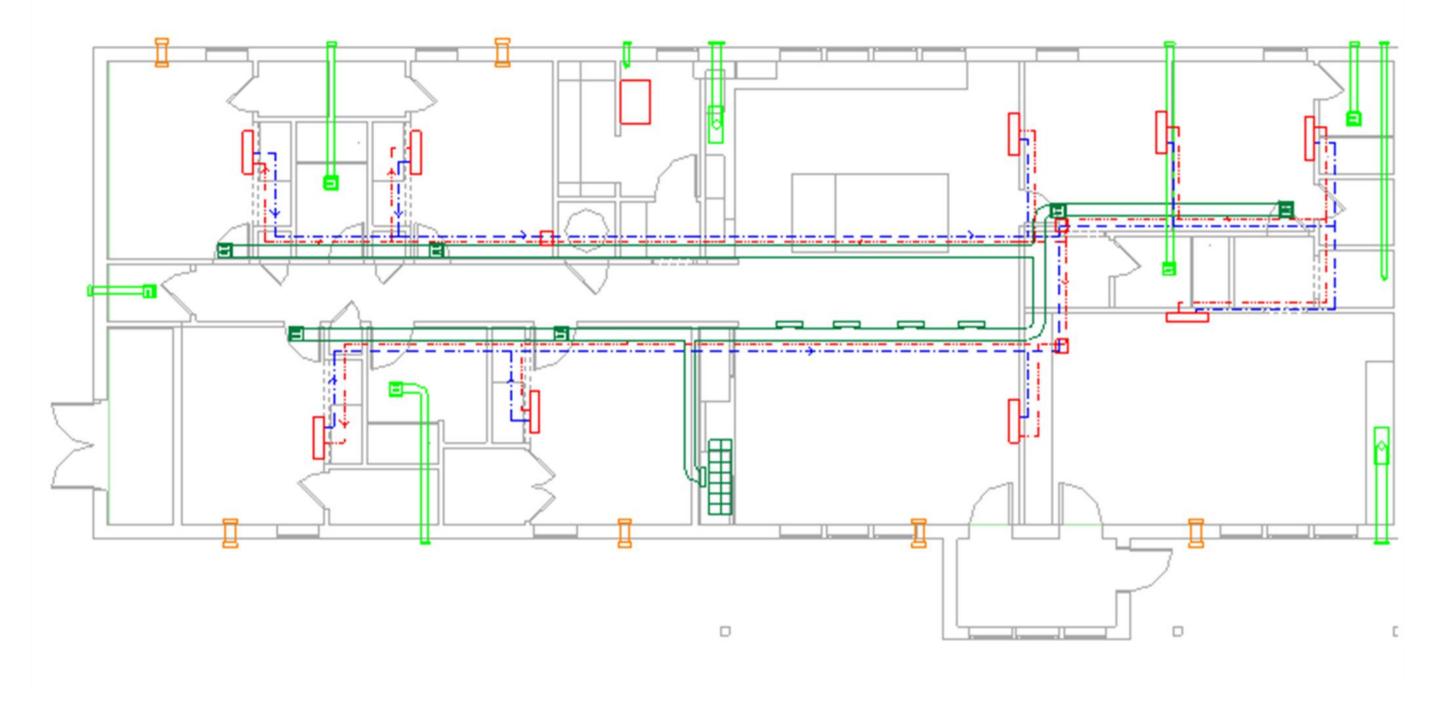
ARK	DOOR TYPE	COMMENTS
00	А	EXT.
01	В	INT.
02	В	INT.
03	C D	INT.
04	D	INT.
05	D	INT.
06	E E	INT.
07	D	INT.
08	В	INT.
09	F	INT.
10A	В	INT.
0B	C C C D	INT.
0C	С	INT.
0D	С	INT.
11A		INT.
1B	D	INT.
2B	D	INT.
2C	D	INT.
2D	D	INT.
13A	В	INT.
3B	C G	INT.
14		INT.
15	G	EXT.
16	Н	EXT.
17	I	EXT.

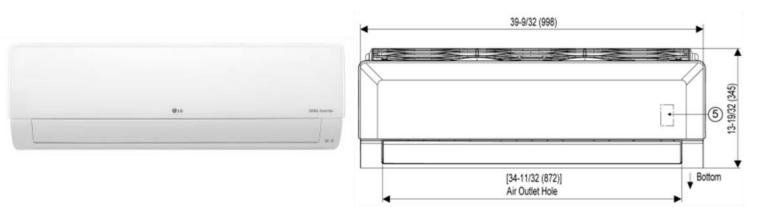
MARK	COMMENTS
A1	Single Hung
A2	Single Hung
В	Fixed
С	Fixed

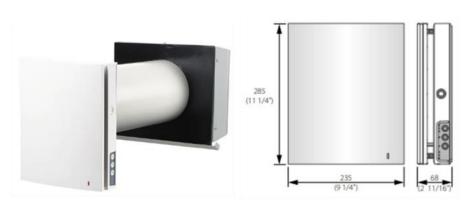
WINDOW SCHEDULE

DOOR SCHEDULE

Mechanical Plan / VRF + Ductless ERV



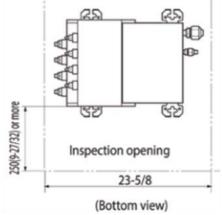




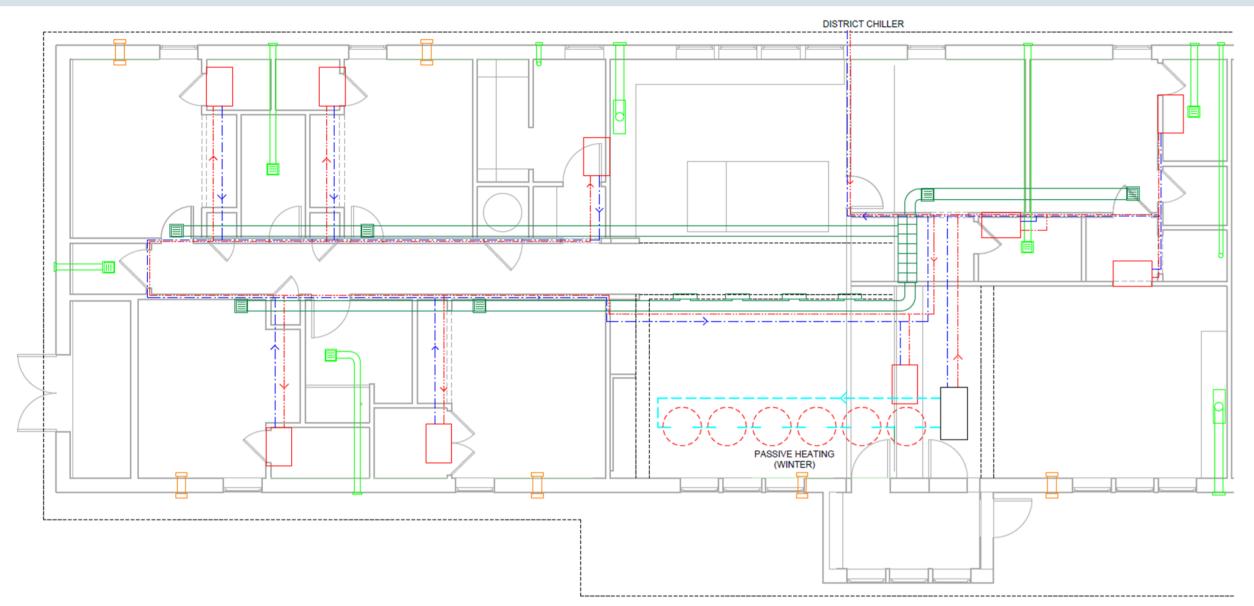
Twin Fresh Expert RHA - 50

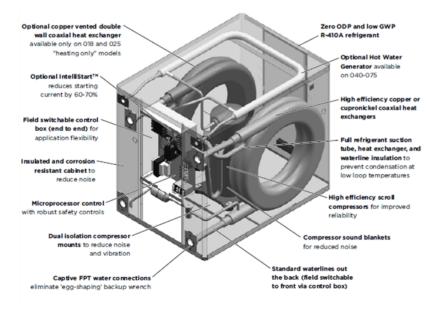






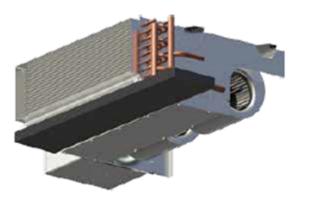
Mechanical Plan / 4-Pipe Fan Coil + Passive Solar + Ductless ERV





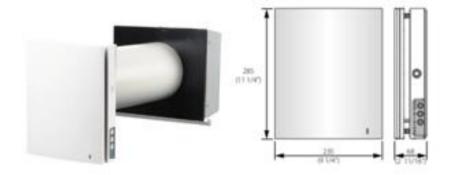


Envision Geothermal Hydronic Heat Pump

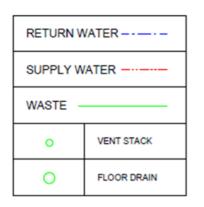


FH Fan Coil Units Low Profile

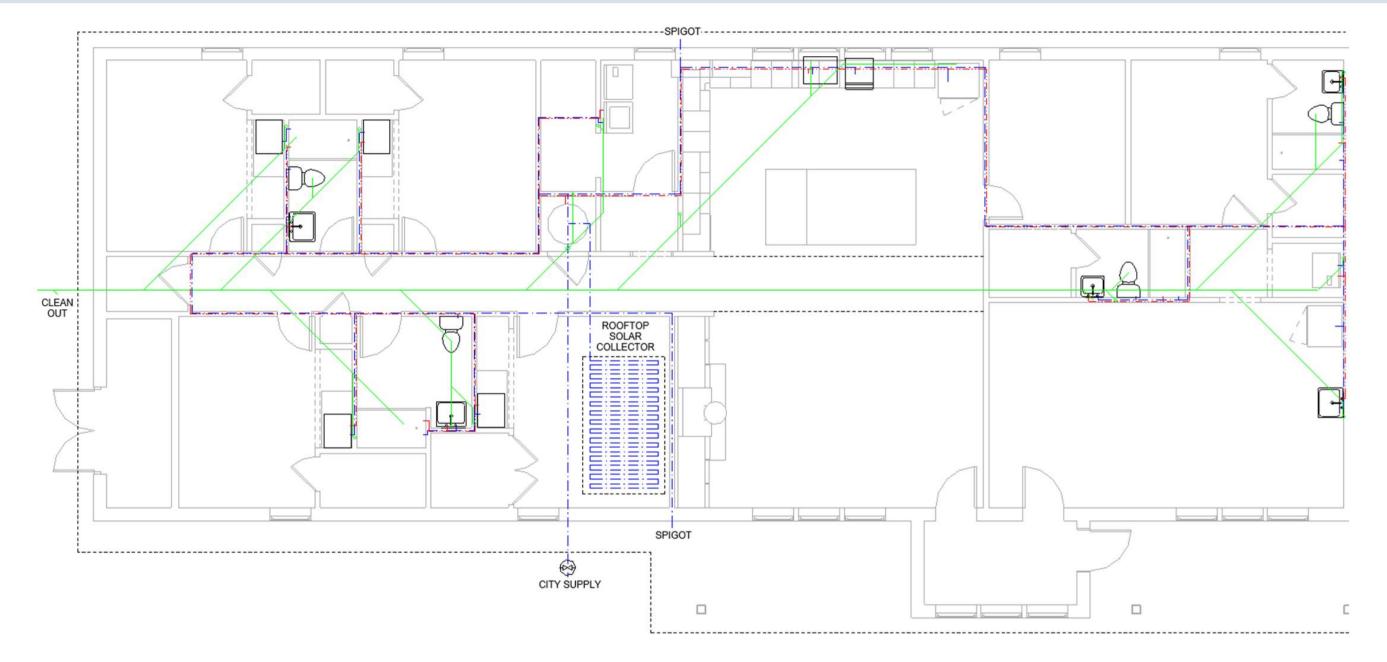
Horizontal Series D



Twin Fresh Expert RHA - 50



Plumbing Plan





H2Optimum 1.1gpf 12" Rough Tank Origin 21 2-handle WaterSense Bathroom Sink Faucet with Drain Niagara Conservation HealthGuard 1.5-gpm Allen + Roth Single Handle Pull-down Kitchen Faucet with Sprayer

COLD WATER							
HOT WATER							
WASTE -	WASTE						
0	O VENT STACK						
0	FLOOR DRAIN						

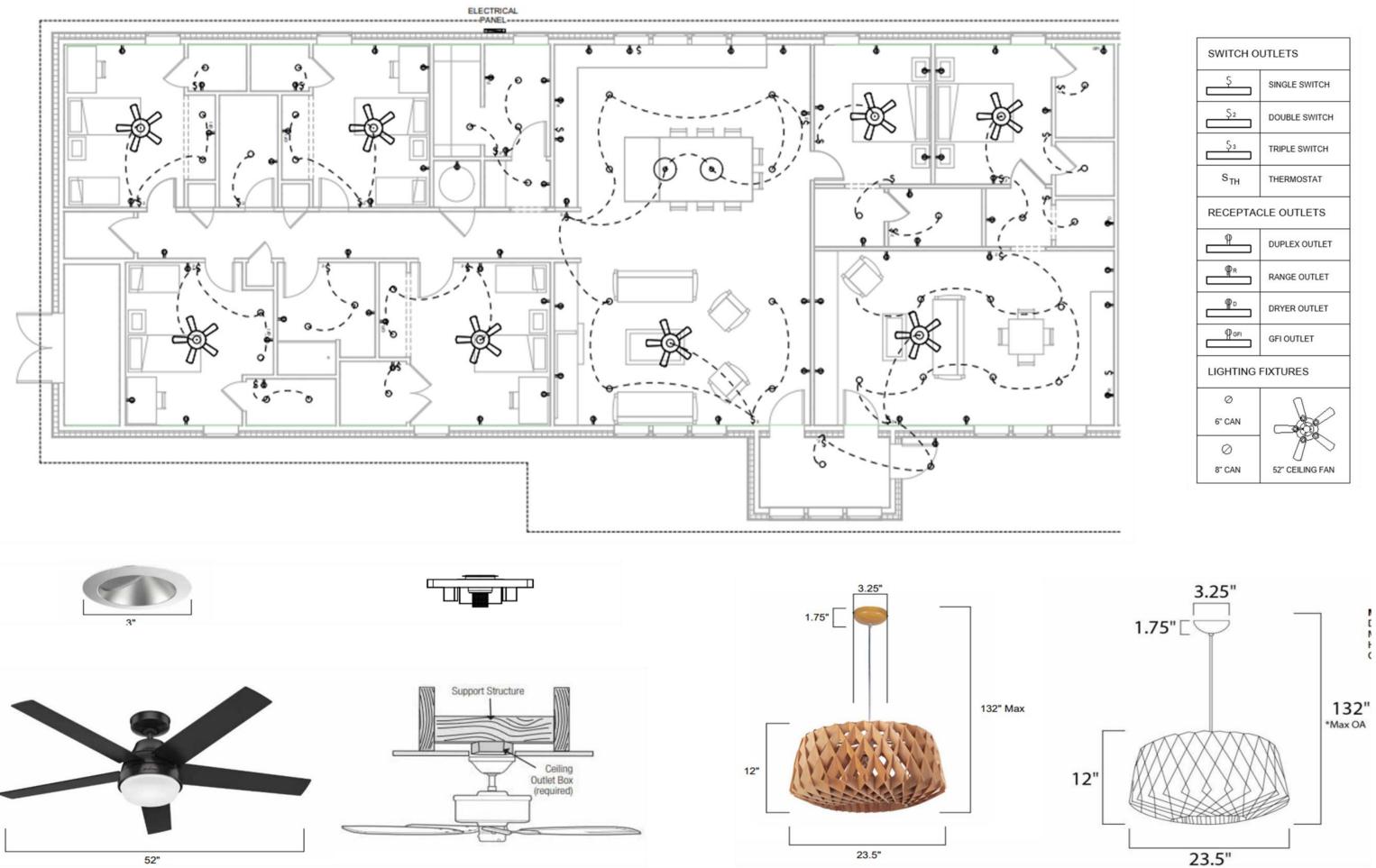
Water Consumption: 110,000 gal/year

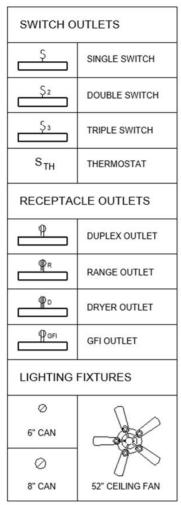




Premium Drinking Water Safe Garden Hose

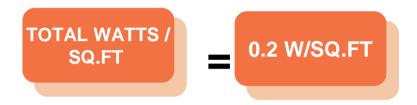
Electrical Plan

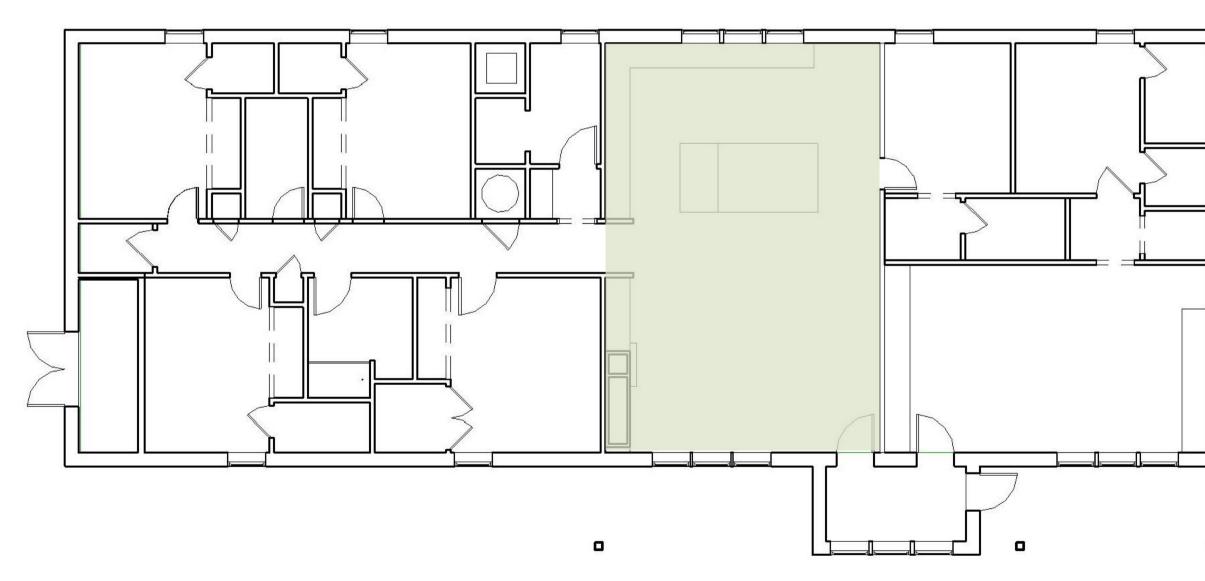




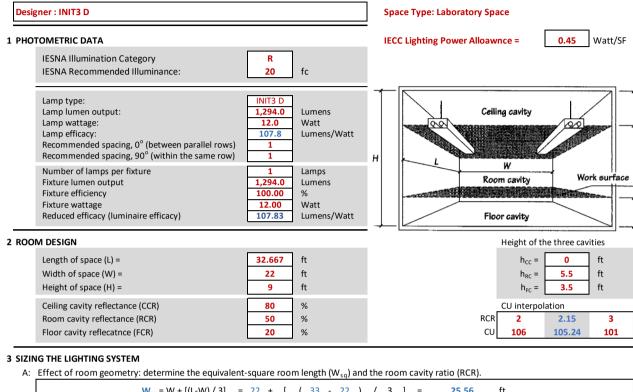
Maxim Horgen Pendant Light

Electric Lighting Design





AVERAGE ILLUMINANCE WORKSHEET - ELECTRIC LIGHTING LUMEN METHOD (SIMPLIFIED)



$W_{sq} = W + [(L-W)/3] =$	= 2	2 +	- [(33	- 22)	/ 3	3]	=	25.56	ft
$RCR = (10 \times H_{RC}) / W_{sq} =$	=	(1	0 x		5.5)	/	25	.56	=	2.15	
According to the photometric data, obtain the Coe	effic	ient	of U	tiliza	ation	(CU) c	of th	is lum	inaire	e in t	the given space	
CU =	=	105.	24%									

B: Effect of maintenance conditions of the space and the system (cleaning, lumen depreciation, relamping, ... etc.)

Light Loss Factor (LLF) =	0.85
---------------------------	------

0.85 for good conditions, 0.75 for average conditions, and 0.65 for poor conditions

C: Calculate useful lumens from one luminaire reaching the workplane

Useful lumens from one luminaire	=	fixture lumen output	x	CU	x	LLF	=			
Useful fumeris from one fumiliare	=	1,294.00	х	1.052	х	0.85	=	1,157.53	Lumens	

D: Calculate total lumens needed on the workplane

Total lumens on the workplane	e Recommended illuminance x space area =							
Total fumeris on the workplane	=	20	x	718.67	=	14,373.48	Lumens	

E: Calculate number of luminaires

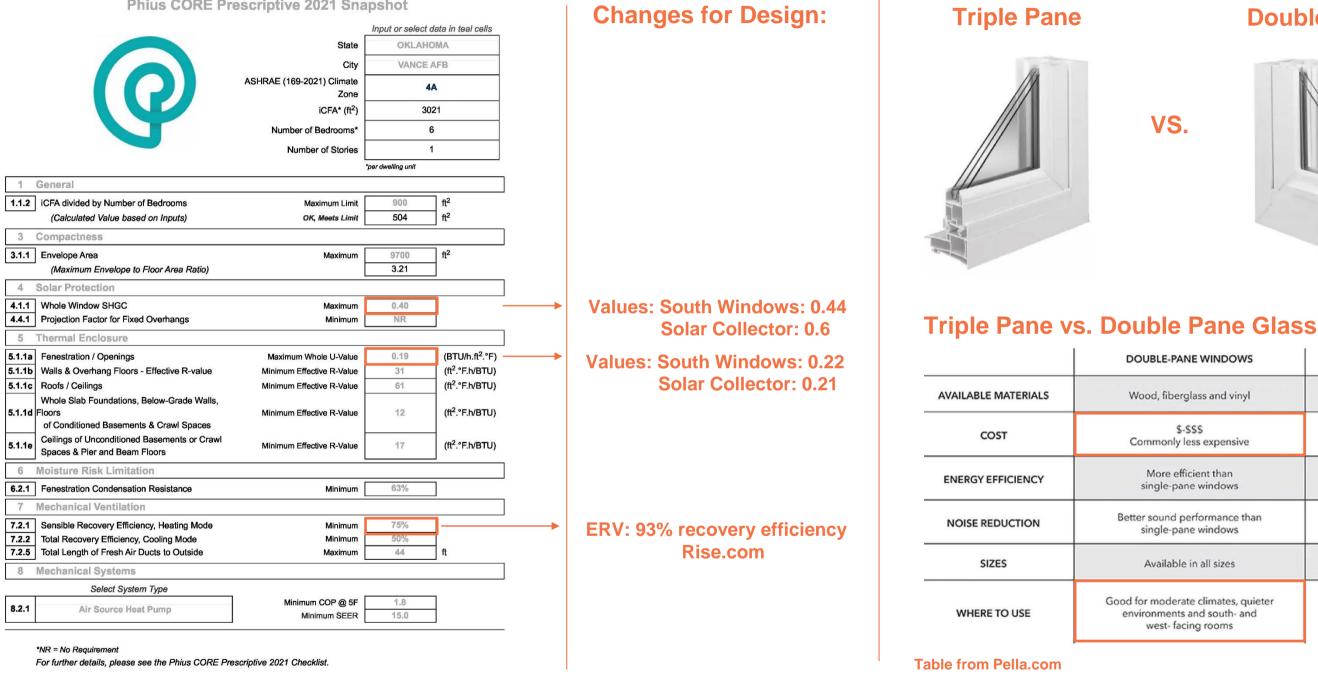
Number of Investories	=	Total lumens on the workplane	/	Useful lumens from one	=		
Number of luminaires	=	14,373.48	/	1,157.53	=	12.42	Luminaires

4 DESIGN EVALUATION

- 31	SILEVALOATION									
	Actual number of luminaires used	=	12							
	Acctual illumination level provided	=	20 x	12	2 /	12	2.42	=	19.33	fc
	Light load	=	12 x	12	2 /	71	8.67	=	0.20	Watt/SF
	Light load index	=	0.2	כ	/	19	.33	=	0.010	Watt/fc.SF
	Floor area covered per luminaire	=	718.	57	/	1	12	=	59.89	SF/Luminaire
	System's overall efficiency	=	100	х	1.05	х	0.85	=	89.45	%

Red text denotes user-provided input data. Last updated October 27, 2022

Passive Solar Heating Information



Phius CORE Prescriptive 2021 Snapshot

Double Pane

VS.



DOUBLE-PANE WINDOWS	TRIPLE-PANE WINDOWS
Wood, fiberglass and vinyl	Wood, fiberglass and vinyl
\$-\$\$\$ Commonly less expensive	\$\$-\$\$\$\$ Commonly more expensive
More efficient than single-pane windows	Most energy efficient
Better sound performance than single-pane windows	Best sound performance
Available in all sizes	Available in all sizes
od for moderate climates, quieter environments and south- and west- facing rooms	Best for extreme climates, noisy places and north- and east-facing rooms

+ Due to the utilization of night insulation, isolated solar heat gain space, roof and wall insulation, and energy recovery ventilator, we were able to choose double pane to save on cost while still be close to the Phius Passive House U-Value of 0.19. The values we chose were 0.21 and 0.22. The value of the SHGC (Solar Heat Gain Coefficient) was originally 0.4. However, we are wanting more solar transmission to the solar heat collector space for the water tubes, so that was increased to 0.6.

Passive Solar Heating / Baseline vs Improved

Average Outdoor Temperature for December 21st : 15.6°F

BEFORE IMPROVEMENTS:

Passive Solar Heating	Calcula	uons, v	vilole Dwelling o	1111, 1501	aleu i leal	Gain		Hillsdale, OH	K	L	December 21
ased on the Balance Point Temperature Metho	od. [Simplified]							Dw	elling unit	envelope load de	ominated building
Location:			Design:			Occ	upancy:	People		Materials:	House
	Hillsdale, OK	36.33 o NL	Total interior area (sq.ft):	3,188.22	Enclosed & Heated	Numb	er of people:	6.00	1	R roof insulation:	61.00
Average outdoor temperature °F:	15.6	December 21	Area of roof (sq.ft):	3,582.17	Insulated	People (E	Btuh/person):	245.00	sensible	R wall insulation:	31.00
			Area of exterior south wall (sq.ft):	813.01	South, including windows	Hours of occ	cupancy/day:	3.00	day-out	U roof:	0.016
Thermostat temperature °F:	72.0		Area of other exterior walls (sq.ft):	1,764.22	All other, including windows			6.50	day-in	U wall:	0.030
			Area of South windows (sq.ft):	144.00	South-facing			8.50	night-awake	U glass:	0.190 d
Orientation:	South		Area of all other windows (sq.ft):	120.00	All other directions			6.00	night-asleep	U glass:	0.190 n
All day solar intensity (Btu/sq.ft):	1,577.6	All day (direct)	Exposed perimeter (ft'):	230.17				Lighting		SHGC of glass:	0.400
	137.7	All day (diffuse)	Net area of south wall (sq.ft):	669.01	Positive value!!!	Light load	d (Watt/sq ft):	0.120		SC of glass:	0.460
Sunshine hours (sunpath diagram):	9.5	Hours	Total area of windows (sq.ft):	264.00	All directions			Equipment	R adde	d night insulation:	0.00
Nighttime hours:	14.5		Net area of exterior walls (sq.ft):	2,313.23	Excluding windows	Equip. load	d (Watt/sq ft):	0.300			Solar Collector
			Gross area of exterior walls (sq.ft):	2,577.23	Including windows			Ventilation		U glass:	0.190 d
	_	To	tal area of exterior walls + roof (sq.ft):	6,159.40	Including windows	Number of	of Bedrooms:	6.00		U glass:	0.190 n
Building's Balance Point Temperature:	34.5	°F	Glass to wall ratio:	10.2%	Dwe	elling Unit Floor	r Area (sq.ft):	3,188.22		SHGC of glass:	0.400
			Envelope-to-floor area ratio:	1.93	(roof + exterior walls) / interio	r area Ventilation	n rate (CFM):	148.1466		SC of glass:	0.460
		S	olar Collector glass-to-floor area ratio:	0.00%	South facing glass / interior a	rea			R adde	d night insulation:	0.000
Required Thermal Mass (Weight of Water_in Ib):	0.0			Solar Collector							Heat recovery
(Volume of Water_in Cubic ft):	0.0		Glass area of Solar Collector (sq.ft):	0.00	South-facing					Heat recovery %:	75.0%

- No Night Insulation •
- **Phius Glass Value Requirements** •
- **No Solar Collector Space** •
- **No Thermal Mass** •

Result: Building's Balance Point Temperature : 34.5 °F > 15.6 °F Code-compliant design cannot provide 100% passive solar heating

AFTER IMPROVEMENTS:

ed on the Balance Point Temperature Metho	d. [Simplified]						Dw	elling unit	[envelope load d	ominated build	ing
Location:			Design:			Occupancy:	People		Materials:	House	1
	Hillsdale, OK	36.33 ° NZ	Total interior area (sq.ft):	3,188.22	Enclosed & Heated	Number of people:	6.00		R roof insulation:	78.35	Í –
Average outdoor temperature °F:	15.6	December 21	Area of roof (sq.ft):	3,582.17	Insulated	People (Btuh/person):	245.00	sensible	R wall insulation:	39.98	
			Area of exterior south wall (sq.ft):	813.01	South, including windows	Hours of occupancy/day:	3.00	day-out	U roof:	0.013	
Thermostat temperature °F:	72.0		Area of other exterior walls (sq.ft):	1,764.22	All other, including windows		6.50	day-in	U wall:	0.023	
			Area of South windows (sq.ft):	144.00	South-facing		8.50	night-awake	U glass:	0.220	day
Orientation:	South		Area of all other windows (sq.ft):	120.00	All other directions		6.00	night-asleep	U glass:	0.108	nigi
All day solar intensity (Btu/sq.ft):	1,577.6	All day (direct)	Exposed perimeter (ft'):	230.17			Lighting		SHGC of glass:	0.330	
	137.7	All day (diffuse)	Net area of south wall (sq.ft):	669.01	Positive value!!!	Light load (Watt/sq ft):	0.120		SC of glass:	0.379	
Sunshine hours (sunpath diagram):	9.5	Hours	Total area of windows (sq.ft):	264.00	All directions		Equipment	R add	ded night insulation:	4.70	
Nighttime hours:	14.5		Net area of exterior walls (sq.ft):	2,313.23	Excluding windows	Equip. load (Watt/sq ft):	0.300			Solar Collector	
			Gross area of exterior walls (sq.ft):	2,577.23	Including windows		Ventilation		U glass:	0.210	day
			Total area of exterior walls + roof (sq.ft):	6,159.40	Including windows	Number of Bedrooms:	6.00		U glass:	0.106	nigh
Building's Balance Point Temperature:	5.0	°F	Glass to wall ratio:	10.2%	Dwelli	ng Unit Floor Area (sq.ft):	3,188.22		SHGC of glass:	0.600	
			Envelope-to-floor area ratio:	1.93	(roof + exterior walls) / interior area	Ventilation rate (CFM):	148.1466		SC of glass:	0.690	
		_	Solar Collector glass-to-floor area ratio:	3.61%	South facing glass / interior area			R add	ded night insulation:	4.700	
Required Thermal Mass (Weight of Water_in lb):	1,564.0			Solar Collector						Heat recovery	
(Volume of Water_in Cubic ft):	25.0		Glass area of Solar Collector (sq.ft):	115.00	South-facing				Heat recovery %:	93.0%	

- **Cellular Shades on Tracks**
- Glass Values: (Utilized Viracon)
- Solar Collector Space
- Thermal Mass

Viracon: 1" (25mm) Insulating with RoomSide Low-E VE13-85



Result: Building's Balance Point Temperature : 15.6 °F (exceeds necessary) Due to the deep overhang, February was the critical month (design condition).

Night Insulation – Double Cell Black Out

Viracon: 1" (25mm) Insulating with RoomSide Low-E VE13-85



Cellular Window Shade: **Double Cell Cellular Window Shades Black** Out on Tracks



Rise:

Energy Recovery Ventilator Vents-US TwinFresh Expert RA1-50-2 Ductless Energy Recovery Ventilator

With an integrated humidity sensor or connection to an external sensor, the unit provides a comfortable microclimate, while the integrated control system ensures easy operation



Passive Solar Heating / Sizing the Systems' Components

Heliodon





The Heliodon was beneficial in determining the percentage of light intake the overhang and window combination. The created model was tracked for every hour of sunlight during the day. We were able to alter the form and distance of windows to bring more light for passive solar heating. .

.....

ased on the Balance Point Temperature Method.		Whole Dwelling Unit, Is			Dwelling unit [envelope I	oad dominated building
Location:		Design:		Occupancy	: People Materia	IS: House
	Hillsdale, OK 36.33 ° NL	-	8.22 Enclosed & Heated	Number of people:		
Average outdoor or design temperature °F:	15.6 February 21	Area of roof (sq.ft): 3,58	2.17 Insulated	People (Btuh/person)	245.00 sensible R wall insula	tion: 43.03
		Area of exterior south wall (sq.ft): 81	3.01 South, including windows	Hours of occupancy/day		roof: 0.016
Thermostat temperature °F:	72.0		4.22 All other, including windows			wall: 0.022
			4.00 South-facing		8.50 night-awake U g	
Orientation:	South		0.00 All other directions		6.00 night-asleep U g	
Unobstructed all day solar intensity (Btu/sq.ft):	1,556.8 All day (direct)		9.01 Positive value!!!	Light lood (Mott/og ft)	Lighting SHGC of g . 0.120 SC of g	
All day solar intensity after shading (Btu/sq.ft):	233.4 All day (direct) 158.9 All day (diffuse)		4.00 All directions	Light load (Watt/sq ft):	Equipment R added night insula	
Sunshine hours (sunpath diagram):	9.5 Hours		3.23 Excluding windows	Equip. load (Watt/sq ft):		Solar Collector
Nighttime hours:			7.23 Including windows	Equip. Ious (Tracing II)	Ventilation U g	
		Total area of exterior walls + roof (sq.ft): 6,15	9.40 Including windows	Number of Bedrooms:	6.00 Ug	lass: 0.103 nig
Building's Balance Point Temperature:	15.6 °F	Glass to wall ratio: 10	0.2% Dwell	ing Unit Floor Area (sq.ft):	3,188.22 SHGC of g	lass: 0.600
		Envelope-to-floor area ratio:	1.93 (roof + exterior walls) / interior area	Ventilation rate (CFM):	: 148.1466 SC of g	
	4 070 0		29% South facing glass / interior area		R added night insula	
Required Thermal Mass (Weight of Water_in Ib): (Volume of Water_in Cubic ft):	1,878.9 22.5	Solar Co Glass area of Solar Collector (sq.ft):	5.00 South-facing		Heat recover	y %: 93.0%
Building Overall Heat Transfer Coefficient					The total building thermal envelope UA = su	m of U-factor times assembl
UA-Building (day)	during day hours (without night	insulation) + ventilation	Btuh/ °F		Formula:	
UA-Roof	3,582.17 sq.ft	0.016 Btuh/sa.ft °F	56.99		7 UA = Area x U	
UA-Net Solid Walls	2,313.23 sq.ft	0.022 Btuh/sq.ft °F	50.42		8 UA = Area x U	
UA-Glazed Windows	2,313.23 sq.it 264.00 sq.ft	0.200 Btuh/sq.ft °F	52.80		UA = Area x U	
UA-Glazed Solar Collector	105.00 sq.ft	0.200 Btuh/sq.ft oF	21.00		UA = Area x U	Solar Co
UA-Exposed Perimeter + Slab	230.17 linear foot	0.07 Btuh/ft °F	16.11		UA = length x U	Exposed Pe
UA-Ventilation (total house)	3,188.22 sq.ft	6.00 bedrooms	7.0% 10.37		2 Vent Rate = 0.03 floor are + (7.5 x no of bedroo	
		Hourly UA (dayti	ime) = 207.69		3	
UA-Building (night)	during night hours (with night in	vsulation) + ventilation	Btuh/ °F			
UA-Roof UA-Net Solid Walls	3,582.17 sq.ft	0.02 Btuh/sq.ft °F	56.99		UA = Area x U	
	2,313.23 sq.ft	0.02 Btuh/sq.ft °F	50.42		UA = Area x U	
UA-Glazed Windows UA-Glazed Solar Collector	264.00 sq.ft 105.00 sq.ft	0.10 Btuh/sq.ft °F 0.10 Btuh/sq.ft °F	27.22		4 UA = Area x U	
UA-Exposed Perimeter + Slab	230.17 linear foot	0.10 Btuh/sq.ft °F 0.07 Btuh/ft °F	10.82		6 UA = Area x U 2 UA = length x U	Solar Co Exposed Pe
UA-Ventilation (total house)	3,188.22 sq.ft		7.0% 10.37		7 CFM x 1.08 x (1-Heat recovery %)	Exposed Pe Ver
		Hourly UA (nightti				
Internal Heat Gain		Average Hourly	/ UA = 186.08 Bit	ıh/ °F	UA = (UA day x day hours) + (UA night x night h	ours)/24 Space
Heat gain (day)	day hours - partially occupied		Btuh			
					Formula:	
People	6.00 people	245.00 Btuh	1,470.00		0	
Equipment	0.30 Watt/sq.ft	3,188.22 sq.ft	3.41 3,261.55		2_q = Power load x area of space x 3.41	Equ
			4,731.55			
Heat gain (night)	night hours - occupied		Btuh		Formula:	
People	6.00 people	245.00 Btuh	1,470.00		g = Number of people x Heat gain from one per	son per hour
Light	0.12 Watt/sq.ft		3.41 1,304.62		g = Light load x area of space x 3.41	
Equipment	0.30 Watt/sq.ft	3,188.22 sq.ft	3.41 3,261.55		g = Power load x area of space x 3.41	Equ
			6,036.17		Accounts for hours o	f sleep at night, with 10% ligh
Solar Heat Gain:		Hourly Aver	rage = 4,858.72 Etc	h 116,609.2	Q = [(q x number of hours) + (q x number of hours)	rs)]/24 Occ
Solar heat gain	during day hours		Btuh		Formula:	
Direct solar (Solar Collector)	1,556.79 Btu/sq.ft	105.00 sq.ft	0.690 4,697.22			rea x SC]/24
Direct solar (South windows)	233.38 Btu/sq.ft	144.00 sq.ft	0.43 595.53		4 Solar Heat Gain = [(all day solar gain) x glass a	rea x SC]/24
Indirect solar (North windows)	158.88 Btu/sq.ft	120.00 sq.ft	0.43 337.86		Solar Heat Gain = [(all day solar gain) x glass a	rea x SC]/24 D
		Hourly Aver	rage = 5,630.61 Bto	h 120,841.8	Solar Heat Gain = direct + diffused	
	~	Polonce Roint (T) The second T	n widi)			
	ro 56.4	Balance Point (T b) = Thermostat Temperature - (Qi / U) °F				
t Balance Point Temperature, Net Thermal Exchange=zei						
t Balance Point Temperature, Net Thermal Exchange=zer $\Delta T = (Q_{\rm i}/UA \ {\rm total})$	56.4	°F		Compare Balance Point 1	remperature to the Average Outdoor Tempera	ature 15.6 °F
t Balance Point Temperature, Net Thermal Exchange=zee ΔT = (Q , / UA total) Thermostat Temperature	56.4 72.0	°F		Compare Balance Point 1	Temperature to the Average Outdoor Temper	ature 15.6 °F February 21
t Balance Point Temperature, Net Thermal Exchange-zee $\Delta T = (2,/UA total)$ Thermostal Temperature Balance Point (7,)	56.4 72.0 15.6	°F °F 'F		Compare Balance Point T	Temperature to the Average Outdoor Temper	
$\label{eq:constraint} \begin{array}{c} \text{Balance Point Temperature, Net Thermal Exchange-zero }\\ & & & & & & & & & & & & & & & & & & $	56.4 72.0 15.6 harvesting according to the loca	°F °F 'F			Temperature to the Average Outdoor Temper	
$\label{eq:constraint} \begin{array}{c} \text{Balance Point Temperature, Net Thermal Exchange-zero }\\ & & & & & & & & & & & & & & & & & & $	56.4 72.0 15.6 harvesting according to the loca Calculate the Solar Heat Gain Factor In testing models H	*F *F F tion, orientation, and unit design. (Al Day), according to the testing of physical models.	Corrected SH		Temperature to the Average Outdoor Temper	
Lealance Point Temperature, Net Thermal Exchange-zer AT = (0, /UA exa) Thermostal Temperature Balance Point (Te) the table below is to quantify the actual daily solar Solar Harvesting	56.4 72.0 15.6 harvesting according to the loca Calculate the Solar Heat Gain Factor	*F *F F ttion, orientation, and unit design. (All Day), according to the testing of physical models.	Corrected SH		Temperature to the Average Outdoor Temper	
Thermostal Temperature Balance Point (7,) he table below is to quantify the actual daily solar Solar Harvesting As obtained from	56.4 72.0 15.6 harvesting according to the loca Calculate the Solar Heat Gain Factor to testing models H % glss	*F *F *F (Al Day), according to the testing of physical models. Iourly SHGF Corrections Clearnee Diffuse (North) Elevation number	Corrected SH	IGF	Assumptions:	
Lealance Point Temperature, Net Thermal Exchange-see AT = (0, /UA exa) Thermostal Temperature Estance Point (T_s) he table below is to quantify the actual daily solar Solar Harvesting As obtained from Fobruary 21 7 AM 8 AM	56.4 72.0 15.6 Calcute the Solar Heat Gain Factor testing models H % glass exposed Direct 0.00% 94	*F *F *F (Al Day), according to the testing of physical models. tourly SHGF Corrections Diffuse (North) Elevation number 3 11 1.000 0.970 11	Corrected SH 55 South 2.8 11.0	IGF Diffuse 2.8 11.0	Assumptions: (1) Thermostat temperature = 72 degrees (2) Shadow patterns per testing models.	
t Balance Point Temperature, Net Thermal Exchange-zee AT = (0 //UA stall) Thermostat Temperature Balance Point (Ts) the table below is to quantify the actual daily solar: Solar Harvesting As obtained from Fobruary 21 7 AM 8 AM 9 AM	56.4 72.0 15.6 harvesting according to the loca Calculate the Solar Heat Gain Factor to testing models to testing models	*F *F *F ttion, orientation, and unit design. (Al Day), according to the testing of physical models. tourly SHGF Corrections Diffuse (North) Elevation number 3 1.000 0.970 11 1.000 0.970 17 1.000 0.970 17 1.000 0.970 17 1.000 0.970 17 1.000 0.970 17 1.000 0.970 17 1.000 0.970 17 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Corrected SH SS 2.8 11.0 16.9	IGF Diffuse 2.8 11.0 16.9	Assumptions: (1) Thermostati temperature = 72 degrees (2) Shadw patients per treating models. (3) Al digas is vertical.	February 21
It Balance Point Temperature, Net Thermal Exchange-zee AT = (0, / UA shall Thermostat Temperature Balance Point (T_s) the table below is to quantify the actual daily solar Solar Harvesting As obtained from Fobruary 21 7 AM 9 AM 10 AM 11 AM	56.4 72.0 15.6 harvesting according to the local Calculate the Solar Heat Gain Factor to sting models H % glass exposed 0.00% 20 0.00% 94 0.00% 197 0.00% 222	"F "F "F TF tion, orientation, and unit design. (Al Day), according to the testing of physical models. tourly SHGF Corrections Diffuse (North) Elevation number 3 1.000 0.970 11 1.000 0.970 11 1.000 0.970 22 1.000 0.970 22 1.000 0.970	Corrected SH 35 South 2.8 11.0 16.9 21.7 23.6	KGF 2.8 11.0 16.9 21.7 23.6	Assumptions: (1) Thermostat temperature = 72 degrees (2) Shadow pattering per testing models. (3) Aligasis is vertical. (4) SHQF correction factors according to ASHR (5) Night insulation is used from survet to survis	AE tables.
$\begin{tabular}{lllllllllllllllllllllllllllllllllll$	56.4 72.0 15.6 harvesting according to the local colspan="2">calculate the Solar Heat Gain Factor to testing models H % glass Direct 0.00% 94 0.00% 94 0.00% 153 0.00% 157 0.00% 222 0.00% 222	*F *F *F (Al Day), according to the testing of physical models. (Al Day), according to the testing of physical models. (A	Corrected SH 35 South 2.8 11.0 16.9 21.7 23.6 24.6	IGF 2.8 11.0 16.9 21.7 23.6 24.6	Assumptions: (1) Thermostat temperature = 72 degrees (2) Shadow patterns per testing models. (3) Adjass is vertical. (4) SHGF correction factors according to ASHR (5) Night insulation is used from surset to surrise (6) Insulating value of wall signes other than insula	AE tables.
It Balance Point Temperature, Net Thermal Exchange-zee AT = (0, / UA shall Thermostat Temperature Balance Point (T_s) the table below is to quantify the actual daily solar Solar Harvesting As obtained from Fobruary 21 7 AM 9 AM 10 AM 11 AM	56.4 72.0 15.6 harvesting according to the local Calculate the Solar Heat Gain Factor to sting models H % glass exposed 0.00% 20 0.00% 94 0.00% 197 0.00% 222	"F "F "F TF tion, orientation, and unit design. (Al Day), according to the testing of physical models. tourly SHGF Corrections Diffuse (North) Elevation number 3 1.000 0.970 11 1.000 0.970 11 1.000 0.970 22 1.000 0.970 22 1.000 0.970	Corrected SH 35 South 2.8 11.0 16.9 21.7 23.6	KGF 2.8 11.0 16.9 21.7 23.6	Assumptions: (1) Thermostat temperature = 72 degrees (2) Shadow pattering per testing models. (3) Aligasis is vertical. (4) SHQF correction factors according to ASHR (5) Night insulation is used from survet to survis	AE tables.
Elalance Point Temperature, Net Thermal Exchangescent AT = (0, /UA exa) Thermostal Temperature Balance Point (Tr) Balance Point (Tr) the table below is to quantify the actual daily solar Scolar Harvesting As obtained from February 21 7 AM 9 AM 10 AM 11 AM 12 NOCN 1 FM 2 PM 3 PM	56.4 72.0 15.6 harvesting according to the local Calculate the Solar Heat Gain Factor testing models H % glass Direct 0.00% 94 0.00% 94 0.00% 94 0.00% 13 0.00% 222 0.00% 242 0.00% 213 15.00% 160	*F *F *F trians orientation, and unit design. (All Day), according to the testing of physical models. (according to the testing of physical models. (according to the testing of physical models. (according to the testing of physical models.) (according to the t	Corrected SH 33 South 2.8 11.0 16.9 23.6 24.6 24.6 24.6 24.4 7.5 34.8	IGF 2.8 11.0 16.9 21.7 23.6 24.6 20.4 17.5 13.6	Assumptions: (1) Thermostat temperature = 72 degrees (2) Shadow patterns per testing modes. (3) Algasis is vertical. (4) SHQF correction factors according to ASHR (5) Night insulation is used from survet to survisi (5) Night insulation is used from survet to survisi (5) Night insulation of the testing and use (7) Insulating value of rol layers other than insul (8) Ventilation is calculated per ASHRAE Standa (9) Heating cortication of DWH beating and use	AE tables. a. b. b. b. b. b. b. b. b. b. b
Balance Point Temperature, Net Thermal Exchange-sce AT = (0, /UA cols) Thermostal Temperatures Estince Point (7s) the table below is to quantify the actual daily solar Solar Harvesting Balance Point (7s) As obtained from Fobruary 21 7 AM 8 AM 9 AM 9 AM 11 AM 12 NOON 1 FM 2 FM 3 FM 4 FM	56.4 72.0 15.6 harvesting according to the local Calculate the Solar Heat Gain Factor to testing models Heat Gain Factor % glass exposed Direct 0.00% 94 0.00% 94 0.00% 197 0.00% 222 0.00% 242 0.00% 243	*F *F *F *F *F *F *F *F *F * * * * * *	Corrected SH 35 South 2.8 11.0 16.9 21.7 23.6 24.6 24.6 24.4 17.5	IGF 2.8 11.0 16.9 21.7 23.6 24.6 20.4 17.5	Assumptions: (1) Thermostat temperature = 72 degrees (2) Stodwo patterns per testing models. (3) Al glass is vertical. (4) SHGF correction factors according to ASHR (5) Night insulation is used from surset to surtifie (5) Insulating value of valid layers other than insul (6) Insulating value of valid layers other than insul (9) Ventilation is accludated per ASHRAE Standa (9) Ventilation is accludated per ASHRAE Standa (9) Astaning contribution of DHW heating and use (9) Cocupants are askeep for 6 hours during ingli	AE tables.
Lealance Point Temperature, Net Thermal Exchange-cent AT = (0, /UA exa) Thermostal Temperature Balance Point (Te) the table below is to quantify the actual daily solar Solar Harvesting As obtained from Fobruary 21 7 AM 8 AM 9 AM 10 AM 11 AM 12 NOCN 1 PM 2 PM 3 PM	56.4 T2.0 15.6 harvesting according to the local catulate the Solar Heat Gain Factor to testing models K V's glass oxposed Direct 0.00% 94 0.00% 94 0.00% 92 0.00% 232 0.00% 242 0.00% 243 0.00% 243 0.00% 213 15.00% 160 85.00% 72	*F *F *F trians orientation, and unit design. (All Day), according to the testing of physical models. (according to the testing of physical models. (according to the testing of physical models. (according to the testing of physical models.) (according to the t	Corrected SH 35 2.8 11.0 16.9 22.7 23.6 24.6 20.4 17.5 34.8 30.0 0.0	IGF 2.8 11.0 16.9 21.7 23.6 24.6 20.4 17.5 13.6 6.8	Assumptions: (1) Thermostat temperature = 72 degrees (2) Shadow patterns per testing modes. (3) Algasis is vertical. (4) SHQF correction factors according to ASHR (5) Night insulation is used from survet to survisi (5) Night insulation is used from survet to survisi (5) Night insulation of the testing and use (7) Insulating value of rol layers other than insul (8) Ventilation is calculated per ASHRAE Standa (9) Heating cortication of DWH beating and use	AE tables.



Analysis: visual representation of the performance of the Dwelling L
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Heat Loss (all day) December 21

Solar Collector Heat Loss

Volume of Water Assumptions: Solar heating raises water

	Total (all day)		
Roof	75,948.8	Btu	31.80%
Net Solid Walls	67,196.2	Btu	28.14%
Glazed Windows	49,769.3	Btu	20.84%
Solar Collector	10,604.3	Btu	4.44%
Exposed Perimeter + Slab	21,473.2	Btu	8.99%
Ventilation	13,821.0	Btu	5.79%
TOTAL Heat Loss	238,812.8	Btu	All Day
			-

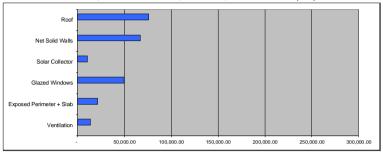
OTAL Heat Loss	238,812.8 Btu	

214,387.5 Btu 10,604.3 Btu 13,821.0 Btu

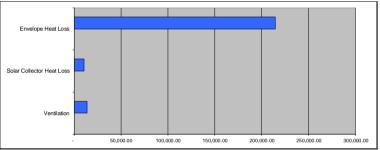
4.44% 5.79%

U Daytime		U Nighttime		ΔΤ	
Btuh/ °F	hours	Btuh/ °F	hours	°F	Total
56.99	9.5	56.99	14.5	55.5	75,948.8
50.42	9.5	50.42	14.5	55.5	67,196.2
52.80	9.5	27.22	14.5	55.5	49,769.3
11.25	9.5	5.80	14.5	55.5	10,604.3
16.11	9.5	16.11	14.5	55.5	21,473.2
10.37	9.5	10.37	14.5	55.5	13,821.0

HEAT LOSS BREAK DOWN, THROUGH ENVELOPE, PERIMETER, AND VENTILATION (BTU).



HEAT LOSS BREAK DOWN, THROUGH ENVELOPE AND VENTILATION (BTU).



Gain (all day)	December	21		1	night hours - occupied	(day hours - partially occupi	ed	
	Total (all day)		_		Btuh	hours	Bt	uh hours	
People	26,460.0	Btu	11.08%		1,470.0	14.50	1,470	0.0 6.50	
Light	11,872.0	Btu	4.97%		1,304.6	14.50	(0.0 6.50	
Equipment	78,277.2	Btu	32.78%		3,261.5	14.50	3,261	.5 9.50	
Solar - Solar Collector	61,201.8	Btu	25.63%					Accounts for	hours of sleep at night, with
Solar - South Windows	53,972.3	Btu	22.60%						
Solar - other directions	7,029.5	Btu (diffuse)	2.94%						
TOTAL Heat Gain	238,812.8	Btu	All Day						
				HEAT GAIN BREAK D	OWN, BY HEAT	SOURCE, I	N ONE DAY (BTU).		
				1					
				People					
				Light					
				Equipment					
				-					
				Solar - Solar Collector					
				Solar - South Windows					
				Solar - other directions					
				-	50,000.00	0 100,00	00.00 150,000.00	200,000.00	250,000.00
				HEAT GAIN BREAK D	OWN. BY HEAT	SOURCE. I	N ONE DAY (BTU).		
							- (-)		
Internal Heat Gain	116,609.2	Btu	48.83%	-					
Internal Heat Gain Solar Heat Gain	116,609.2 122,203.6	Btu Btu	48.83% 51.17%						
Solar Heat Gain	122,203.6	Btu							
Solar Heat Gain	122,203.6	Btu		Internal Heat Gain					
Solar Heat Gain	122,203.6	Btu		Internal Heat Gain					
Solar Heat Gain	122,203.6	Btu		Internal Heat Gain					
Solar Heat Gain	122,203.6 122,203.6 116,609.2	Btu		Internal Heat Gain					
Solar Heat Gain Solar Heat Gain Internal Heat Gain	122,203.6 122,203.6 116,609.2	Btu		Internal Heat Gain					
Solar Heat Gain Solar Heat Gain Internal Heat Gain Required Thermal Mass	122,203.6 122,203.6 116,609.2 238,812.8	Btu		Internal Heat Gain					
Solar Heat Gain Solar Heat Gain Internal Heat Gain	122,203.6 122,203.6 116,609.2 238,812.8	Btu							

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250,000.00 Last updated 02/12/2024

300.00

150,000.00

100,000.00

50 000 00

200,000.00

Passive Cooling / Natural Ventilation

Thermostat Temp = 85°F

LIVING ROOM:

		Type of space: R	esidential		Location: Hillsdale	, ОК	Month:	May, 21st		All exterior wal	s, roofs and win	dows are shaded
				IECC CI	imate Zone: 4A						No impact of so	ol-air temperature
										Solar heat gain	s due to diffused	l component only
STEP 1: INPU	T DATA	Time of day:	12:00	Military time						Outside	e temperature is	lower than inside
	Location	n & Climate:					Design	:		Occupancy:		
	Outsid	e Air Temperature	83.0	°F		Area of space	•		sq.ft.	Number of people	1.0	person(s)
		ain Factor (diffuse)		Btuh/sq.ft			height of space			Metabolism		Btuh/person
	Wind Speed ((at weather station)	35.0	mph (from h	ourly data)	Gross area of the	wind-facing wall	90.00	sq.ft.	Light load	0.12	W/sq.ft
Wind Effectiveness	Factor (due to d	context and height)	0.55	(from Figure	1) Area	of the wind-facing	glazed windows	18.00	sq.ft. (note 2)	** Equipment load	0.30	W/sq.ft
Wind Eff	ectiveness Fact	or (due to azimuth)	0.55	(read note 1)	* Area of g	lazed windows no	facing the wind	0.00	sq.ft.			
						Shading Coefficie	nt of glass (SC)	0.46	(note 3)***	Thermostat temperature	85.0	°F
	Effective Wind	Speed at Window	10.59	mph		Windo	w type (air inlet)	Single-Hung				
						Sta	ck height (if any)	14.00	ft			
					Тој	p-of-stack opening	type (air outlet)	Jalousie				
STEP 2:												
HEAT GAIN (a	it the desig	gn condition)										
										Formula:		
	Windows'	solar heat gain	37.50	Btuh/sq.ft	18.00 sq.ft.	0.46		310.50	Btuh		= SHGF x	Glass area x S
	Sol	id Walls & Roof	NA		NA			NA	Btuh	ignor	ed if all walls and	d roof are shade
		People	1.00	person(s)	245.00 Btuh			245.00	Btuh		= number x me	etabolism of eac
		Lights	170.00	sq.ft.	0.12 Watt/sq.ft	3.41		69.56	Btuh		= area x	k light load x 3.4
		Equipment	170.00	sq.ft.	0.30 Watt/sq.ft	3.41		173.91	Btuh		= area x equip	ment load x 3.4
	Total	Peak Heat Gain						798.97	Btuh		= SUM o	of all of the abov

Cross Ventilation:

Works with ambient temp of 83 degrees F

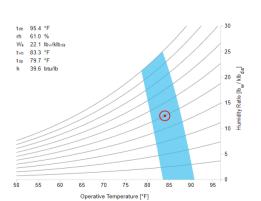
Complies with ASHRAE Standard 55-2020





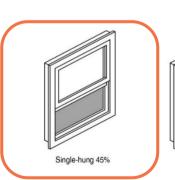
Cools space when wind speeds inadequate Up to 83 degrees F

Air is drawn in from windows and exhausted through stack. A fan array proportionally activates based on how many spaces turn on their inlet fans.



Ceiling Fan:





Standard

BEDROOMS:

	Type of space:	Residential		Location:	Hillsdale,	ок	Month:	May, 21st		All exterior walls, r	oofs and wind	dows are shaded
			IECC Cli	mate Zone:	4A					No	o impact of so	l-air temperature
										Solar heat gain is d	ue to diffused	component only
STEP 1: INPL	JT DATA Time of day:	12:00	Military time							Outside ter	mperature is l	lower than inside
	Location & Climate:						Design	:		Occupancy:		
	Outside Air Temperature	83.0	°F			Area of space	(to be ventilated)	685.00	sq.ft.	Number of people	6.0	person(s)
	Solar Heat Gain Factor (diffuse)	37.5	Btuh/sq.ft			Average	e height of space	9.00	ft.	Metabolism	245.0	Btuh/person
	Wind Speed (at weather station)	35.0	mph (from ho	ourly data)	0	Gross area of the	wind-facing wall	260.00	sq.ft.	Light load	0.12	W/sq.ft
Wind Effectivenes	s Factor (due to context and height)	0.55	(from Figure	1)	Area o	f the wind-facing	glazed windows	54.00	sq.ft. (note 2)*	* Equipment load	0.30	W/sq.ft
Wind Ef	fectiveness Factor (due to azimuth)	0.55	(read note 1)	*	•		ot facing the wind		· ·			
					5	Shading Coeffici	ent of glass (SC)	0.46	(note 3)***	Thermostat temperature	85.0	°F
	Effective Wind Speed at Window	10.59	mph				ow type (air inlet)					
							ack height (if any)		ft			
					Тор	-of-stack openin	g type (air outlet)	Jalousie				
STEP 2:												
HEAT GAIN (a	at the design condition)										
										Formula:		
	Windows'solar heat gain	37.50	Btuh/sq.ft	81.00	sq.ft.	0.46		1,397.25	Btuh		= SHGF x	Glass area x S
	Solid Walls & Roof	NA		NA				NA	Btuh	ignored i	f all walls and	l roof are shade
	People	6.00	person(s)	245.00	Btuh			1,470.00	Btuh	=	number x me	tabolism of eacl
	Lights	685.00	sq.ft.	0.12	Watt/sq.ft	3.41		280.30	Btuh		= area x	light load x 3.4
	Equipment	685.00	sq.ft.	0.30	Watt/sq.ft	3.41		700.76	Btuh	=	area x equip	ment load x 3.4
	Total Peak Heat Gain	·						3,848.31	Btuh		= SUM c	f all of the above

Outdoor Temperature = 83 °F

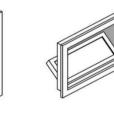








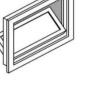
Double-hung 45%



Sliding 45%



Hopper 45%



Casement 90%



Top of Stack

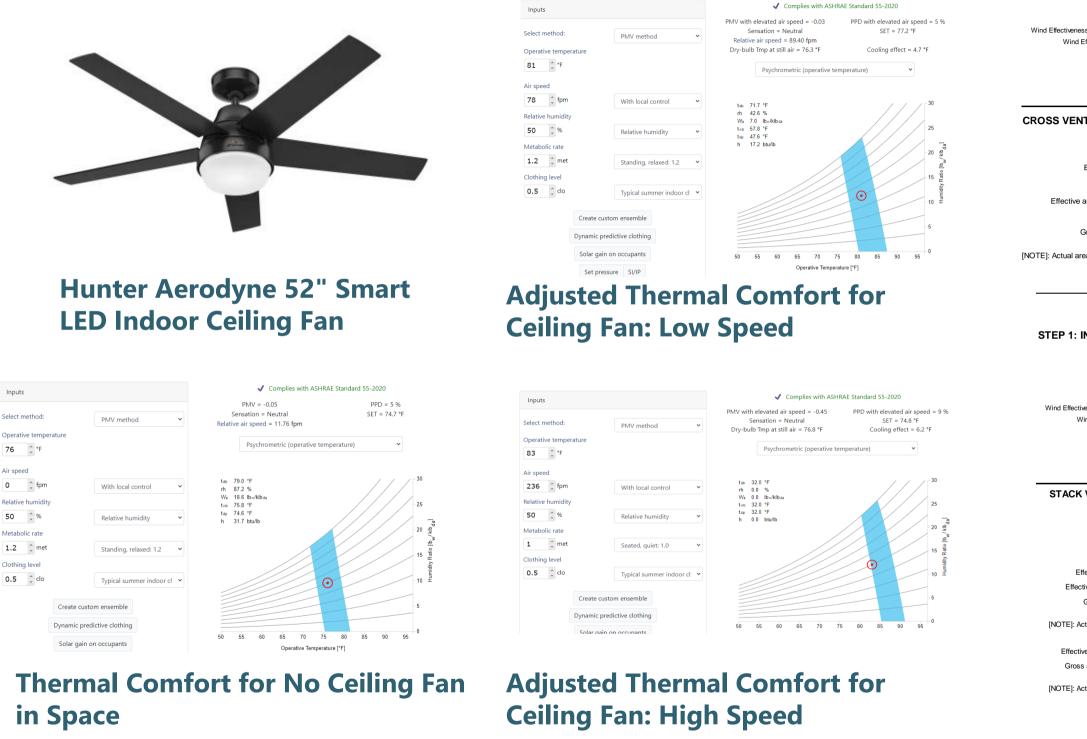
Jalousie 75%

Kitchen

Natural Ventilation / Sizing

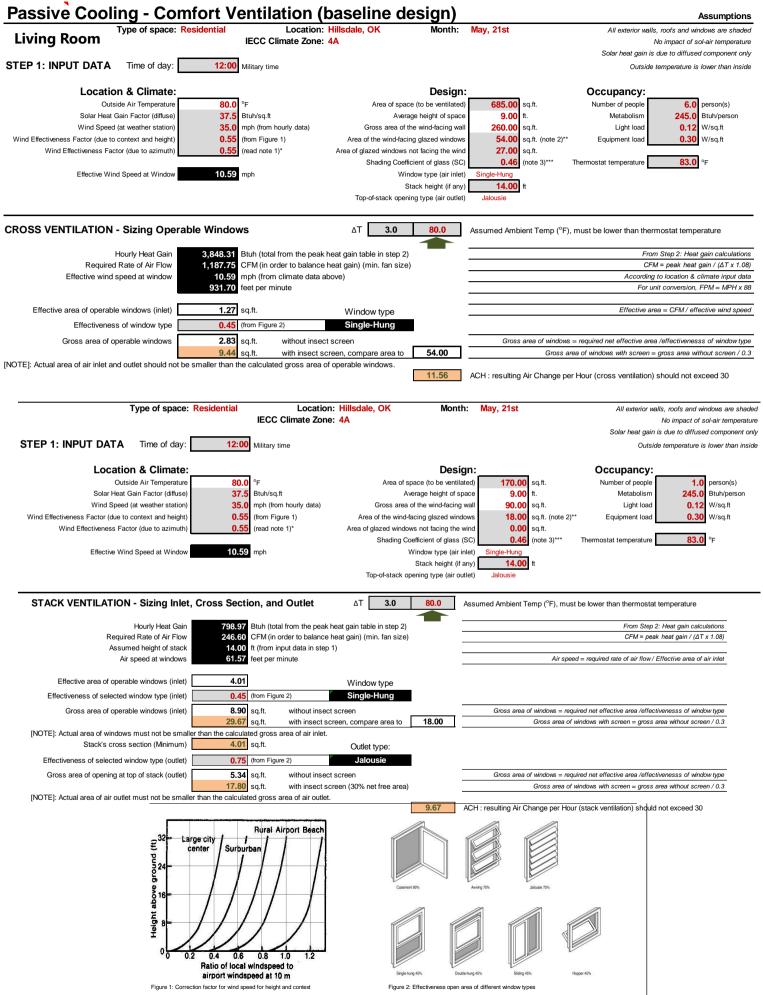
Living Room

Wind Effectiveness Eactor (due to context and heigh



Inputs

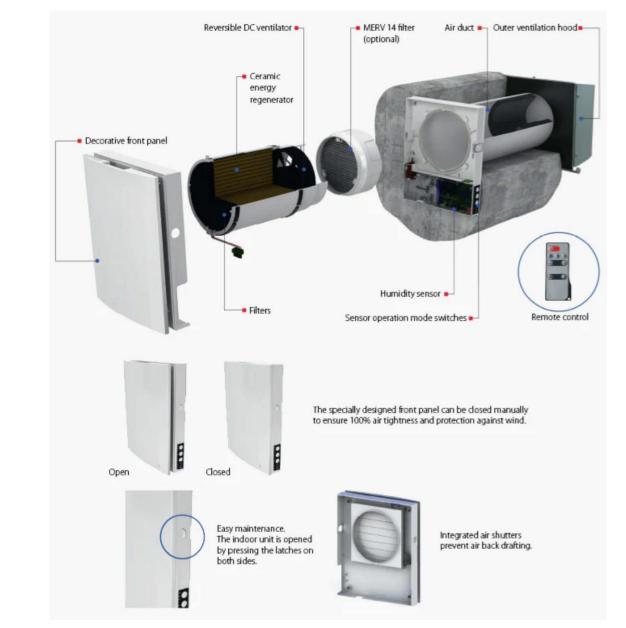
Air speed



Source of figure 1: Cooling with Ventilation, Chandra et al, Florida Solar Energy Center, 1986, page 30 .

Energy Recovery Ventilator Information

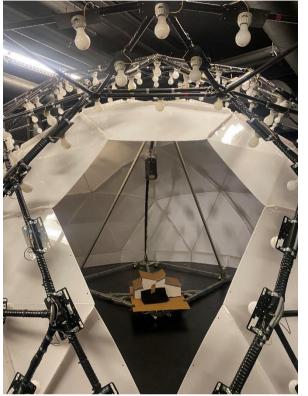
Specifications				-
Room Size	One TwinFresh Expert unit in ventilation mod 2016	de can serve rooms up to 500 sq. ft in accor	dance with ANSI/ASHRAE Standard 62.2-	
Features	Unique Single Room Energy Recovery Ver One TwinFresh Expert unit in ventilation n Communication between several ventilate Efficient supply and exhaust single-room High-tech ceramic energy regenerator wi Reversible DC motors with low energy de Integrated humidity sensor or connection Integrated control system. Silent operation from 0.3 Sones. Easy mounting and maintenance. Air cleaning with total MERV 5 class filters Rated for continuous operation. Frost- and condensate-free.	node can serve rooms up to 500 sq. ft*. ars for coordinated operation. ventilation up to 30 CFM. th max. heat recovery efficiency up to 93 % mand from 3.61 W and safe voltage of 12 V to external sensor for comfortable microd	l.	 Serves up to rooms up to 500 sq. ft Efficient supply and exhaust single-room ventilation Silent Operation from 0.3 Sones
Speed	1	2	3	
Voltage / 50 (60) Hz [V]	1-100-240			
Power consumption [W]	3.61	4.15	5.20	
Current consumption [A]	0.025	0.030	0.039	
Air flow in ventilation mode [CFM]	9	18	30	
Air flow in regeneration mode [CFM]	4	9	15	
RPM	800	1300	1900	
Sound pressure level @ 3 ft [Sones]	0.6	1.0	1.2	
Sound pressure level @ 10 ft [Sones]	0.3	0.5	0.6	
Outdoor sound pressure attenuation [Sones]	2.5			
Transported air temperature ["F]	from +5 up to +104			
Regeneration efficiency [%]	max. 93			ERV: 93% recovery efficiency
Regenerator type	Ceramic			
Filter	MERV 5 (option: MERV 14)			
MINIMUM WALL THICKNESS	S 7/8"			
Ingress protection	IP24			



up to 30 CFM.

Daylight Analysis

Artificial Sky Dome

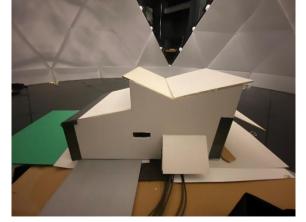




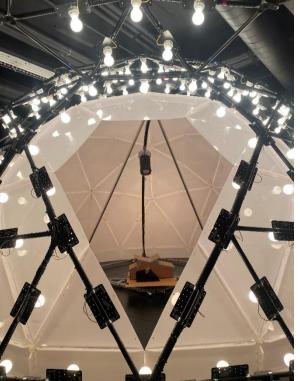
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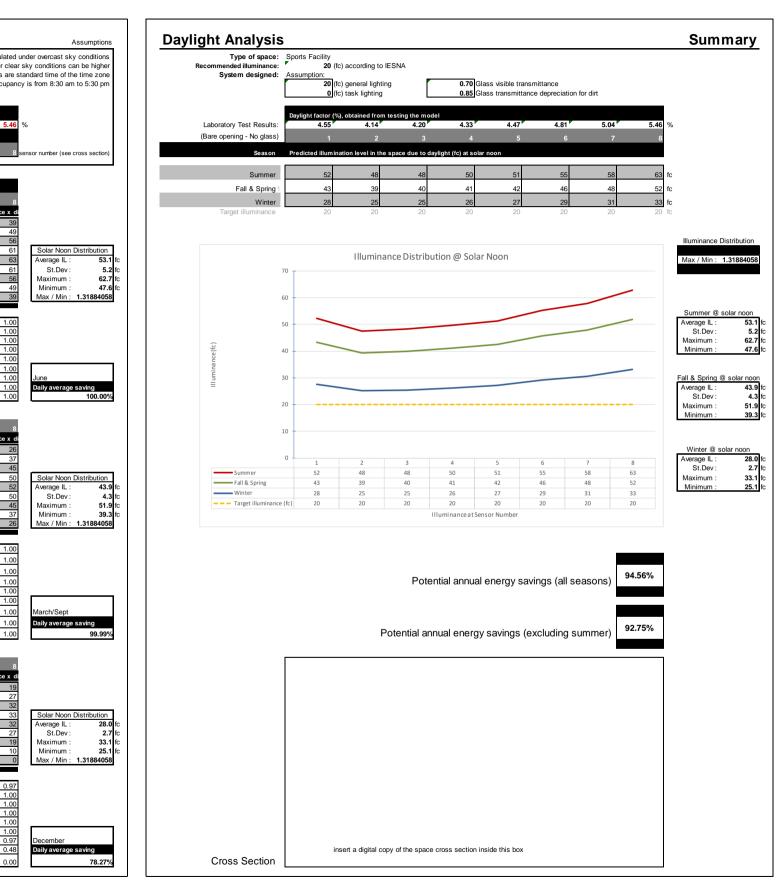
The Artificial Daylighting Dome was an integral component in designing an even level of illuminance distribution within the central living space. Several tests were examined to alter the form and window openings.





l yr Recommended	be of space: I illuminance:	Sports Facility 20	(fc) according to					Potential saving Savi	g is calculate ngs under cle
	n designed:	Assumption: 20	(fc) general lighting	ting		Glass visible tra Glass transmitt			Hours are Occupa
			(%), obtained fro			4.47	1.01	5.04	
	Test Results: ng - No glass)	4.55 Points as desir	4.14 gnated in the mo	4.20	4.33	4.47	4.81	5.04	5.4
		1	2	3	4	5	6	7	
		Coloulated proc	licted illuminand	o – oputdoor ot	ondord illumino				
						IICE X DF X glas	S VI X LLF		
21		Points as desig	nated in the mo	aeia on cross se 3	action 4	5	6	7	
Outsi	de illuminance							x glass visible tra	nsmittance x
9 a.m. 10 a.m.	1208 1508	33 41	30 37	30 38	31 39	32 40	35	36 45	3
11 a.m.	1738	47	43	43	45	46	50	52	5
12 p.m.	1882	51	46 48	47 48	48 50	50	54	56 58	6
1 p.m. 2 p.m.	1931 1882	52 51	40	40	50 48	51 50	55 54	56	6
3 p.m.	1738	47	43	43	45	46	50	52	E
4 p.m. 5 p.m.	1508 1208	41	37 30	38 30	39 31	40 32	43	45 36	4
lar noon @ 1:00			ight saving (%) :						
	9 a.m.	Potential dayl	ight saving (%) : 1.00	= [actual illumina 1.00	ance from dayl	ght / required ill 1.00	uminance] ≤100 1.00	1.00	1.0
	10 a.m.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
	11 a.m. 12 p.m.	1.00	1.00 1.00	1.00	1.00	1.00	1.00	1.00	1.0
	1 p.m.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
_	2 p.m.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
	3 p.m.	1.00	1.00 1.00	1.00	1.00	1.00	1.00	1.00	1.0
	4 p.m. 5 p.m.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
/Sept 21		1	2	3	4	5	6	7	
Outsi 9 a.m.	de illuminance 809	Predicted illum	ination level in th 20	ne space due to c 20	daylight (fc) = st	andard outside il 22	luminance x DF	x glass visible tra 24	nsmittance x
10 a.m.	1135	31	20	20	21	30	32	34	
11 a.m.	1386	38	34	35	36	37	40	42	4
<u>12 p.m.</u> 1 p.m.	<u>1544</u> 1597	42	38 39	39 40	40 41	41 42	44 46	46 48	5
2 p.m.	1544	42	38	39	40	41	44	46	5
3 p.m.	1386	38	34	35	36	37	40	42	4
4 p.m. 5 p.m.	1135 809	31 22	28 20	28 20	29 21	30 22	23	34 24	2
ar noon @ 1:00	pm	Potential day	ight saving (%) :	= [actual illumin;	ance from davli	aht / required ill	uminancel < 100	1%	
	9 a.m.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
	10 a.m.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
	11 a.m.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
	12 p.m.								1.0
		1.00	1.00	1.00	1.00	1.00	1.00	1.00	
_	1 p.m. 2 p.m.	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.0
-	1 p.m.	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.0
	1 p.m. 2 p.m. 3 p.m. 4 p.m.	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00	1.0 1.0 1.0 1.0
	1 p.m. 2 p.m. 3 p.m.	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.00 1.00 1.00	1.0 1.0 1.0
	1 p.m. 2 p.m. 3 p.m. 4 p.m.	1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00	1.0 1.0 1.0 1.0
	1 p.m. 2 p.m. 3 p.m. 4 p.m.	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 5	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 7	1.0 1.0 1.0 1.0 1.0
	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m.	1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 2 ination level in the set of	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 4 Jaylight (fc) = st 15	1.00 1.00 1.00 1.00 1.00 5	1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 7 x glass visible trai 18	1.0 1.0 1.0 1.0 1.0
9 a.m. 10 a.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. de illuminance 595 825	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 2 ination level in tt 15 20	1.00 1.00 1.00 1.00 1.00 3 as space due to 15 21	1.00 1.00 1.00 1.00 1.00 1.00 4 Jaylight (fc) = str 15 21	1.00 1.00 1.00 1.00 1.00 5 andard outside if 16 22	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 7 x glass visible tra 18 25	1.0 1.0 1.0 1.0 1.0
Outsi 9 a.m. 10 a.m. 11 a.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. de illuminance 595 825 970	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1 Predicted illum 16 22 22 26	1.00 1.00 1.00 1.00 1.00 1.00 2 ination level in tt 15 20 20 24	1.00 1.00 1.00 1.00 1.00 3 e space due to o 15 21 24	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 5 andard outside ii 16 22 26	1.00 1.00 1.00 1.00 1.00 1.00 6 Iuminance x DF 17 24 28	1.00 1.00 1.00 1.00 1.00 7 x glass visible tra 18 25 25 29	1.0 1.0 1.0 1.0 1.0
Outsi 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. de illuminance 595 825 970 1019 970	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 4 daylight (fc) = sti 25 26 26 25	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Outs 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 60 illuminance 595 825 970 1019 970 825	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 4 Jaylight (fc) = st 15 21 25 26 25 26 25 21	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 7 x glass visible tra 18 25 25 29 31 29 29 25	1.0 1.0 1.0 1.0 1.0
Outsi 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. de illuminance 595 825 970 1019 970	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 4 daylight (fc) = sti 25 26 26 25	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 7 x glass visible trat 18 25 29 31 29 25 18	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Outs 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 5 p.m. 6 Turrinance 595 825 970 1019 970 825 595 296 0 0	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Outst 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 5 p.m. 6 Turrinance 595 825 970 1019 970 825 595 296 0 0	1.00 1.00 1.00 1.00 1.00 1.00 Predicted illum Predicted illum 22 26 28 28 26 28 28 26 28 26 28 20 16 28 28 26 26 20 20 20 26 28 26 26 26 20 20 20 26 26 26 26 26 26 26 26 26 26	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 24 25 24 25 24 25 24 25 24 7 7	1.00 1.00 1.00 1.00 1.00 1.00 15 21 24 25 24 24 24 21 7 7 0	1.00 1.00 1.00 1.00 1.00 4 Jaylight (fc) = str 15 21 25 26 25 21 15 26 25 8 0	1.00 1.00 1.00 1.00 1.00 5 andard outside if 16 22 26 22 26 27 26 27 26 27 26 28 8 0	1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 x glass visible trai 8 25 29 31 28 29 31 29 25 18 29 31 29 31 0 20 26 0 0	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Outst 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 5 p.m. 6 iluminance 595 825 970 1019 970 825 595 296 0 0 0 pm	1.00 1.00	1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 3 as space due to c 15 21 24 24 25 24 24 21 15 7 0 = [actual illumin. 0.74	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 7 x glass visible tra 18 28 28 29 31 31 29 25 5 18 9 0 0	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Outs 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 5 p.m. 6 iluminance 595 825 970 1019 970 825 595 595 296 0 0 pm 9 0 a.m. 10 a.m.	1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 24 25 24 20 24 20 15 7 7 0 0 15 0 0 15 0 0 0 15 0 0 0 0 0 0 0 0 0 0 0 0 0	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 4 daylight (fc) = st 21 25 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 0.0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.00 1.00 1.00 1.00 1.00 5 andard outside if 16 22 266 27 26 222 16 8 8 0 29 16 0 29 16 20 20 16 20 20 16 20 20 10 20 20 20 20 20 20 20 20 20 2	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 17 24 28 29 28 24 17 8 29 28 24 17 8 29 28 24 17 8 29 28 24 17 25 17 24 17 24 28 29 28 28 24 17 17 24 28 29 28 28 29 28 28 24 17 17 24 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 28 29 28 29 28 28 29 28 28 29 28 28 29 28 29 28 29 28 29 28 28 29 29 28 29 29 28 29 29 28 29 29 29 20 20 20 20 20 20 20 20 20 20	1.00 1.00 1.00 1.00 1.00 x glass visible training of the second sec	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Outs 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 5 p.m. 6 iluminance 595 825 970 1019 970 825 595 296 0 0 0 pm	1.00 1.00	1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 3 as space due to c 15 21 24 24 25 24 21 15 7 0 = [actual illumin. 0.74	1.00 1.00	1.00 1.00	1.00 1.00	1.00 1.00 1.00 1.00 1.00 x glass visible trai 25 29 25 18 29 25 18 9 0 0 % 0.89 1.00	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Outs 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 5 p.m. 6 iluminance 595 825 970 1019 970 825 595 6 296 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 1 1 1 a.m. 1 a.m.	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 Potential dayl 0.81 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 24 25 24 20 24 20 15 7 0 0 15 0 0 15 0 0 15 0 0 0 15 0 0 0 0 0 0 0 0 0 0 0 0 0	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 25 24 24 21 15 21 25 24 24 21 15 25 24 24 25 24 24 25 24 24 25 24 24 25 24 24 25 24 24 21 15 25 24 24 25 24 24 21 15 25 24 24 21 15 25 24 24 21 15 25 24 24 21 15 25 24 21 15 25 24 24 21 15 25 24 24 21 15 25 24 24 21 15 27 15 27 10 25 24 24 21 15 27 10 25 24 24 21 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 10 10 10 10 10 10 10 10 10	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 15 21 25 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 27 15 26 27 15 26 27 15 26 27 15 26 27 15 26 27 15 26 27 15 27 15 26 27 15 27 15 26 27 15 27 15 26 27 15 27 15 26 27 15 27 15 26 27 15 27 15 27 15 27 15 27 15 27 15 26 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 10 0 10 0 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 ght / required ill 0.79 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 x glass visible transverse 29 31 29 25 18 9 0 0 1.00	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Onisi 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m. 3 p.m. 4 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 5 p.m. 5 p.m. 68 (Uminance) 595 825 970 1019 970 0 825 595 296 0 0 0 0 0 9 0 9 0 0 0 0 9 0 9 0 0 0 9 0 9 0 0 0 9 0 0 0 9 0 9 0 0 0 9 0 9 0 0 0 9 0 9 0 0 9 0 9 1 1 1 1	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 Predicted illom 1.00 22 26 28 26 28 26 28 26 28 26 28 26 28 26 28 26 28 26 28 26 28 26 28 26 28 26 28 20 20 20 20 20 20 20 20 20 20	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 24 25 24 25 24 20 15 7 7 0 15 20 0 24 25 24 20 15 7 7 0 0 1.00	1.00 1	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Outsi 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 5 p.m. 5 p.m. 5 p.m. 5 p.m. 5 p.m. 1019 970 1019 970 825 595 296 0 0 pm 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 3 p.m.	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 Potential dayl 0.81 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 24 25 24 25 24 20 15 7 0 15 7 0 15 20 0 15 20 0 15 20 0 15 20 0 15 20 0 24 25 24 25 24 20 15 20 0 15 20 0 24 25 24 25 24 25 24 25 24 25 24 20 0 15 20 0 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 25 24 20 0 15 15 7 7 0 0 0 0 0 0 0 0 0 0 0 0 0	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 24 25 24 21 15 21 25 24 24 21 15 21 25 24 24 21 15 25 24 24 25 24 24 25 24 24 25 24 24 25 24 24 25 24 24 21 15 25 24 24 25 24 24 21 15 25 24 24 21 15 25 24 24 21 15 25 24 24 21 15 25 24 21 15 25 24 24 21 15 25 24 24 21 15 25 24 24 21 15 27 15 27 10 25 24 24 21 15 27 10 25 24 24 21 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 15 27 10 10 10 10 10 10 10 10 10 10	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 15 21 25 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 25 21 15 26 27 15 26 27 15 26 27 15 26 27 15 26 27 15 26 27 15 26 27 15 27 15 26 27 15 27 15 26 27 15 27 15 26 27 15 27 15 26 27 15 27 15 26 27 15 27 15 27 15 27 15 27 15 27 15 26 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 15 27 10 0 10 0 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 ght / required ill 0.79 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 x glass visible transverse 29 31 29 25 18 9 0 0 1.00	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0
Outsi 9 a.m. 10 a.m. 11 a.m. 12 p.m. 1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m.	1 p.m. 2 p.m. 3 p.m. 4 p.m. 5 p.m. 5 p.m. 5 p.m. 68 (Uminance) 595 825 970 1019 970 0 825 595 296 0 0 0 0 0 9 0 9 0 0 0 0 9 0 9 0 0 0 9 0 9 0 0 0 9 0 0 0 9 0 9 0 0 0 9 0 9 0 0 0 9 0 9 0 0 9 0 9 1 1 1 1	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 Predicted Illum 1.00 22 266 222 1.00 1.00 0 Potential dayl 0.081 1.00 1.00 0.01 0.00 0.01 0.00 0.0	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 24 25 24 25 24 20 15 7 7 0 15 20 0 24 25 24 20 15 7 7 0 0 1.00	1.00 1	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 0.79	1.00 1.00	1.00 1.00 1.00 1.00 1.00 1.00 1.00 7 x glass visible tra 18 25 29 31 28 25 18 9 0 0 .00 1.00 1.00 1.00 1.00 0.88	1.0 1.0 1.0 1.0 1.0 1.0 1.0 1.0





Summarized Model Inputs

						Ekot	rope						Open Studio	
		Model 1			Model 2			Model 3		Model 4			Model 5	
	A1	A2	Total	A1	A2	Total	A1	A2	Total	A1	A2	Total	Total	
HERS	70	73		50	55		21	27		26	27			
Site EUI	31.7	41.6	34.0	19.7	8.2	27.9	8.8	4.1	12.9	11.7	18.0	13.1	Before PV = 9.64 After P	V = -2.81
Energy Demand														
Total kWh	21718	8394	30112	17479	7255	24734	7796	3665	11461	7973	3639	11612	Before PV = 8540 After P	V = -248
Heating E Demand	9083	2606	11689	4496	1328	5824	441	70	511	577	52	629	141	
Cooling E Demand	2327	880	3207	1970	800	2770	1099	474	1573	1140	466	1606	800	
Hot Water E Demand	3938	1666	5604	3938	1666	5604	0	0	0	0	0	0	0	
Lights + Appliances E Demand	6371	3243	9614	7076	3461	10537	6256	3122	9378	6256	3122	9378	7619	
Renewables														
Photovoltaic Panels	-	-	-	-	-	-	-	-	-	-	-	-	7 kw DC system (22 pa	nels)
Heating Furnace		Furnace			Ductless Mini-Split			Ductless Mini-Split			Water to Water Heat Pump			
Heating Efficiency - HSPF 7.7		9.2			15.8			15.8			15.4			
Cooling	ooling AC Unit			AC Unit			Ductless Mini-Split			Ductless Mini-Split			Air to Water Heat Pu	mp
Cooling Efficiency - SEER				16			18.35			18.35			19.92	
Hot Water	Sta	andard (Elect	tric)	Standard (Electric)			Solar (+ Electric Backup)			Solar (+ Electric Backup)			Solar (+ Electric Back	up)
Tank Size (gallons)		80		80			80			80			80	
Ventilation	Ir	nfiltration Or	nly	Balanced			ERV			ERV			ERV	
Ventilation (cfm)				115	36	151	126	36	162	126	36	162	162	
Wattage				115	36	151	29	8.3	37.3	29	8.3	37.3	37.3	
Lights + Appliances														
Lights	10	0% Fluoresc	ent	100% Fluorescent			100% LED			100% LED			100% LED + Improvements	
Appliances	Н	ERS Referen	се	Н	ERS Referen	ce	Н	ERS Referen	ce	HERS Reference			Energy Star + Improver	nents
Envelope														
Roof R-Value		R-32			R-60		R-62		,	R-65			R-65	
Wall R-Value				R-32		R-35		R-43			R-43			
Glazing U-Value		U-0.50			U-0.30			U-0.19		U-0.20			U-0.20	
Glazing SHGC		0.3			0.4			0.4			0.37		0.37	
Slab R-Value		R-1			R-10			R-13			R-14		R-14	

Site vs. Source Energy

 $Energy_{source} = Energy_{site} * Conversion Factor_{site to source}$ $Energy_{source, Final} = 11,541 \, kWh/yr * 2.21 = 25,506 \, kWh/yr$ $Energy_{source, Final+} = 8,540 \, kWh/yr + 2.21 = 18,874 \, kWh/yr$

	Baseline 1		Baseline 2		Baseline 3		Fir	nal	Final +		
Unit	A1	A2	A1	A2	A1	A2	A1	A2	A1	A2	
HERS	70	73	50	55	21	27	26	27	n/a	n/a	

	Baseline 1	Baseline 2	Baseline 3	Final	Final +
Unit	A1 + A2	A1 + A2	A1 + A2	A1 + A2	A1 + A2
Site EUI	34.0	27.9	12.9	13.1	9.64
Source EUI	75.1	61.7	28.5	29.0	21.3

HERS Ratings

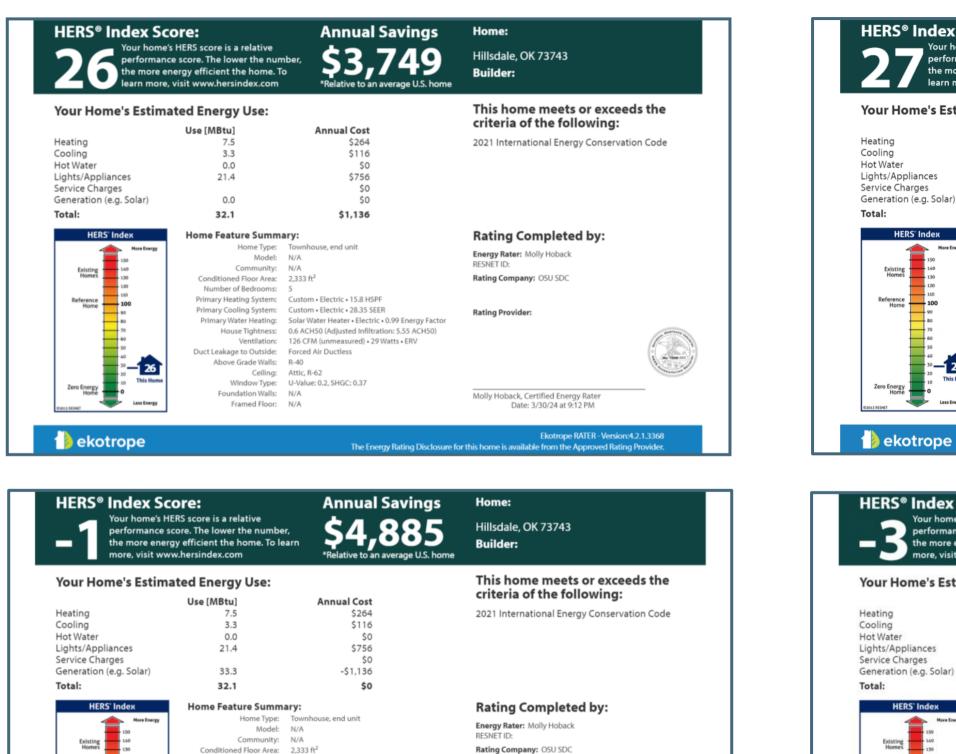
Reference Home

Zero Energy Home

ekotrope

100

-1



140 Existing Homes Conditioned Floor Area: 2,333 ft² Number of Bedrooms: 5 Primary Heating System: Custom • Electric • 15.8 HSPF Reference Home 100 Primary Cooling System: Custom • Electric • 28.35 SEER Primary Water Heating: Solar Water Heater • Electric • 0.99 Energy Factor House Tightness: 0.6 ACH50 (Adjusted Infiltration: 5.55 ACH50) Ventilation: 126 CFM (unmeasured) • 29 Watts • ERV Duct Leakage to Outside: Forced Air Ductless Above Grade Walls: R-40 Ceiling: Attic, R-62 Window Type: U-Value: 0.2. SHGC: 0.37 Zero Energy Foundation Walls: N/A Framed Floor: N/A ekotrope

Ekotrope RATER - Version:4.2.1.3368 The Energy Rating Disclosure for this home is available from the Approved Rating Provider.

Molly Hoback, Certified Energy Rate Date: 3/30/24 at 9:05 PM An. 1998

Rating Provider:

core:	Annual Savings	Home:
e's HERS score is a relative nce score. The lower the n energy efficient the home e, visit www.hersindex.cor	⋼⋰ ⋛ ╏ ℊ ∠ / Э	Hillsdale, OK 73743 Builder:
nated Energy Use:		This home meets or exceeds the
Use [MBtu]	Annual Cost	criteria of the following:
0.1	\$5	2021 International Energy Conservation Code
1.1	\$39	2021 International Energy Conservation Code
0.0	ŝo	
10.7	\$377	
10.7	\$0 \$0	
0.0	ŝo	
11.9	\$421	
-	•	
Home Feature Sum		Rating Completed by:
Home Type		Energy Rater: Molly Hoback
Mode		RESNET ID:
Community		Rating Company: OSU SDC
Conditioned Floor Area Number of Bedroom		Rating Company: 050 SDC
Primary Heating System		
Primary Cooling System		Rating Provider:
Primary Water Heating		Rating Provider.
House Tightnes	: 0.6 ACH50 (Adjusted Infiltration: 0.46 ACH50)	WORTCASE IN
Ventilation		
Duct Leakage to Outside		X No. The Action
Above Grade Walls		a state of the sta
Ceiling Window Type		"Egyption
Foundation Walls		Multi-Malanda Card Ond Farmer Datas
Framed Floo		Molly Hoback, Certified Energy Rater Date: 3/30/24 at 10:42 PM

Ekotrope RATER - Version:4.2.1.3368 The Energy Rating Disclosure for this home is available from the Approved Rating Provider.

ne's Hi ance so e energ	OPE: ERS score is a relative core. The lower the numbe gy efficient the home. To le w.hersindex.com		Home: Hillsdale, OK 73743 Builder:
stima	ated Energy Use:		This home meets or exceeds the
		Annual Cost	criteria of the following:
	Use [MBtu]		2021 Jahren Hinnel Franzis Grander Hinn Golde
	0.1	\$5	2021 International Energy Conservation Code
	1.1	\$39	
	0.0	so	
	10.7	\$377	
	12.2	\$0	
r)	13.3	-\$421	
	11.9	\$0	
	Home Feature Summ	ary:	Rating Completed by:
Energy	Home Type:	Townhouse, inside unit	
	Model:	N/A	Energy Rater: Molly Hoback
	Community:	N/A	RESNET ID:
	Conditioned Floor Area:	688 ft ²	Rating Company: OSU SDC
	Number of Bedrooms:	1	
	Primary Heating System:	Custom • Electric • 15.8 HSPF	
	Primary Cooling System:		Rating Provider:
	Primary Water Heating: House Tightness:		
	Ventilation:		
	Duct Leakage to Outside:		
	Above Grade Walls:		A view and
	Ceiling:	Attic, R-62	In and the second of
	Window Type:	U-Value: 0.2, SHGC: 0.37	
-3	Foundation Walls:		Molly Hoback, Certified Energy Rater
latigne	Framed Floor:	N/A	Date: 3/30/24 at 9:08 PM

EUI Performance Summary

	House Parents Attached Housing Schedules								Guest	Room	Maternity House Schedules						
	Occu	pancy	Occup	bancy	Equip	oment	Li	ghting	Occupancy			Occupancy	Occupancy	Equipment	Lighting	5	
	Living &	Kitchen	Bedro	oms	Living &	Kitchen	'ing & Kito	ch Bedrooms	Living &	Kitchen		Living & Kitchen	Bedrooms	Living & Kitchen	Living & Kitchen	Bedrooms	
Hours	Weekday	Weekend	Weekday	Weekend	Weekday	Weekend	Weekend	ds Weekends	Weekday	Weekend	Hours	All Days	All Days	All Days	All days	All days	
0	0	0	1	1	0.02	0.02	0.1	0.1	0	1	0	0	1	0.02	0.1	0.1	
1	0	0	1	1	0.02	0.02	0.1	0.1	0	1	1	0	1	0.02	0.1	0.1	
2	0	0	1	1	0.02	0.02	0.1	0.1	0	1	2	0	1	0.02	0.1	0.1	
3	0	0	1	1	0.02	0.02	0.1	0.1	0	1	3	0	1	0.02	0.1	0.1	
4	0	0	1	1	0.02	0.02	0.1	0.1	0	1	4	0	1	0.02	0.1	0.1	
5	0	0	1	1	0.02	0.02	0.1	0.1	0	1	5	0	1	0.02	0.1	0.1	
6	0	0	1	1	0.02	0.02	0.1	0.1	0	1	6	0	1	0.02	0.1	0.1	
7	1	1	0	1	0.1	0.02	0.1	0.1	0	0	7	0	1	0.02	0.1	0.1	
8	0	1	0	0	0.02	0.1	0.1	0	0	0	8	0.6	0.2	0.1	0.1	0.1	
9	0	1	0	0	0.02	0.04	0.4	0	0	0	9	0.6	0.2	0.02	0.4	0.1	
10	0	0.7	0	0	0.02	0.04	0.4	0	0	0	10	0.6	0.2	0.2	0.4	0.1	
11	0	0.7	0	0	0.02	0.15	0.4	0	0	0	11	0.6	0.2	0.2	0.4	0.1	
12	0	1	0	0	0.02	0.15	0.4	0	0	0	12	0.6	0	0.2	0.4	0.1	
13	0	0.5	0	0	0.02	0.15	0.4	0	0	0	13	0.8	0	0.04	0.4	0.1	
14	0	0.5	0	0	0.02	0.04	0.4	0	0	0	14	0.8	0	0.04	0.4	0.1	
15	0	0.5	0	0.4	0.02	0.04	0.4	0	0	1	15	0.6	1	0.04	0.4	0.1	
16	0	0.5	0.27	0.4	0.02	0.04	1	0	0	1	16	0.6	1	0.04	1	0.1	
17	0	0.5	0.27	0.4	0.02	0.04	1	0.4	0	0	17	0.8	0.2	0.04	1	0.1	
18	1	0.5	0.27	0.27	0.04	0.04	1	0.4	0	0	18	0.8	0.2	0.2	1	0.4	
19	1	1	0.27	0.27	0.15	0.15	1	0.4	0	0	19	0.8	0.2	0.15	1	0.4	
20	1	1	0.27	0.27	0.2	0.2	0.4	1	0	0	20	0.8	1	0.2	0.4	1	
21	0.5	0.5	0.27	0.27	0.02	0.02	0.1	0.1	0	0	21	0.8	1	0.1	0.1	1	
22	0	0	1	1	0.02	0.02	0.1	0.1	0	1	22	0.1	1	0.02	0.1	0.1	
23	0	0	1	1	0.02	0.02	0.1	0.1	0	1	23	0	1	0.02	0.1	0.1	